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Effect of different loading conditions at evaporators of different temperatures on thermal performances of VCRS using environmental friendly refrigerants using multiple evaporators with compressors of individual types and expansion valves of multiple types

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Abstract

The effect of different loading conditions at different evaporator temperatures on the thermal performances of VCRS using environmentally friendly refrigerants using multiple evaporators with compressors of individual types and expansion valves of multiple type shave has yet to be studied in detail so far in the literature. This paper mainly deals with the detailed first law performance in terms of COP and exergy performance of low GWP refrigerants in multiple evaporators; compressors of individual types used in VCR systems have been studied in detail, and the effect of different evaporators load variations at different evaporators temperatures on thermal performances have been investigated.

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1. Introduction

One of the cruelest environmental issues affecting our planet is global warming. One of its sources is the initial creation of refrigerant gases and carbon dioxide emissions. These gases contribute to global warming because they are released into the atmosphere and stay there for prolonged periods. Based on their life cycle analysis and the effectiveness of refrigeration systems, these gases' environmental effects can be classified according to their severity. Over the next 100 years, Earth's temperature is anticipated to increase due to global warming. This will impact agriculture, resulting in heavy rains, more heat waves, and a possible rise in sea level during the next century. Due to this, the Montreal Protocol's signatory nations decided in 2016 to phase down HFCs and HCFCs to prevent

the ozone layer from being damaged by global warming and reduce net Earth warming by 0.5 °C by the year 2100. Chlorofluorocarbons (CFCs) and hydrochlorofluorocarbons (HCFCs) both destroyed the ozone layer after the Montreal and Kyoto Protocols, respectively [1].

Currently, HFCs like R134a, R23, R404A, R407A, R410A, R125, and R507A make up most of the various refrigerants used in residential, automotive, commercial, and industrial refrigeration and air-conditioning systems. HFCs have a high global warming potential (GWP) despite having no ozone depletion potential (ODP). The GWP of R134a is 1430, that of R23 is 14800, that of R404A is 3922, that of R410A is 2088, that of R407A is 2107, and that of R507A is 3985.

The commercial VCR systems, such as centrifugal chillers and central air conditioning systems used in buildings, use the

HCFC refrigerant (R22), and the current generation uses R134a and R123. R22 is under the A1 safety rating for refrigerants, which means it has a high GWP of 1810 but very low toxicity and no flame propagation. A widely used refrigerant for several kinds of refrigeration systems is R134a. It has a higher safety rating than A1 and is less poisonous, does not spread fire, and has a GWP of roughly 1430.

It is an HFC and will be completely phased out by 2034. R123 is an HCFC molecule with a B1 classification used in chillers because of its excellent thermal efficiency and low risk of leaks. However, because long-term inhalation of R123 has been linked to pancreatic and liver tumors, it is expected to be phased out by 2025.

The USA's Environmental Protection Agency (EPA) has planned to gradually phase out HFCs to 50% by 2025, 80% by 2030, and 100% by 2040 due to the high GWP values of the fourth generation of refrigerants [2]. Therefore, a drop-in replacement for R134a on VCRS with a variable speed compressor and input parameters of the evaporator and condenser temperature has been discovered. This replacement refrigerant should have a low GWP for little environmental impact. HFC-134a provides 3% to 5% higher COP than R404a (COP). Similar to R134a, R410a and R407c have 1% to 1.5% poorer COP efficiency. The outcomes demonstrated that the COP (energy) efficiency (COP) was reduced with R1234yf to 5 to 10% and raised with R1234ze(Z) from 3 to 7% [3]. The thermal performances of VCR systems using R152a are 2 to 6% higher than those using R134a. It was observed that the input power of R152a was 7.724%, 7.72% and 7.752% less than that of R134a, and the COP of the system using R1224yd(Z) showed a 2.35%, 3.15% and 4.95% improvement at compressor speeds of 2000, 2500 and 3000 rpms, respectively, as compared to R134a [4-10]. The HFO-1234yf and HFO-1234ze (E) and R1234ze(Z), R1243zf, R1224yd(Z), R1225ye(Z), R1233zd(E), HFO-1336mzz(Z) were analysed as potential replacements for R134a and the results showed that R1234ze(E) and R1243zf showed the closest performance to R134a. Compared to R1234ze(E) [11-16]. The suitability of eight HFO refrigerants, such as HFO-1234yf and HFO-1234ze(E), as potential alternatives to R134a, was studied using the EES software and showed that these refrigerants improved performance without significantly increasing the GWP [17-21]. The use of R1233zd(E), R1224yd (Z) and R1234ze (Z) in terms of first law efficiency to be around 1%, was better than R245fa [22-29].

COP and exergy performance of low GWP refrigerants in multiple evaporator compressors of individual types used in VCR systems have been studied in detail, and the effect of different load variations on evaporators at separate evaporators' temperatures on thermal performances have been investigated.

2. Results and Discussion

Thermal Performances of VCR systems using HFO-1234ze refrigerant using multiple evaporators at different temperatures with compressors of individual types and expansion valves of

multiple types of using ($T_{eva1}=263K$, $T_{eva2}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$, $Q_{eva1} = 70$ “kW”, $Q_{eva2} = 105$ “kW”, $Q_{eva3} = 35$ “kW”) shown in table-1(a) respectively.

Table-1(a): Validation of thermal performances of VCR systems using HFO-12 refrigerant using multiple evaporators at different temperatures with individual compressors & expansion valves of multiple types for ($T_{eva1}=263K$, $T_{eva2}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$, $Q_{eva1} = 70$ “kW”, $Q_{eva2} = 105$ “kW”, $Q_{eva3} = 35$ “kW”)

| S.N. | Performance Parameters | Ref [29] | Model | % variation |
|------|-----------------------------|----------|-------|--------------------|
| 1 | COP (Ideal) | 6.25 | 6.485 | 3.76 |
| 2 | Total compressor Work “kW” | 33.6 | 32.38 | -3.631 (Reduction) |
| 3 | First compressor Work “kW” | 12.82 | 12.87 | 0.39 |
| 4 | Second compressor Work “kW” | 13.88 | 12.82 | 7.637 |
| 5 | Third compressor Work “kW” | 6.9 | 6.689 | -3.058 (Reduction) |

It was found that the developed model validates under an accuracy of less than 7.64%. The different load conditions are shown in table-1(b), and the other temperature conditions of evaporators Table -1(c), respectively.

Ideal thermal performances of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions are shown in Table-2(a) to Table-2(f), respectively. It was found that the VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions of $Q_{eva1} = 35$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$ kW give maximum COP with lowest electrical energy consumption in terms of total compressors work for running whole system. In contrast, maximum exergy efficiency was found in different load conditions of $Q_{eva1} = 105$ kW, $Q_{eva2} = 70$ kW, and $Q_{eva3} = 35$ kW with maximum electrical energy consumption in terms of total compressors work for running the whole system. However best first law efficiency (COP) of VCR systems using multiple evaporator compressors of individual types with expansion valves for numerous kinds using HFO-1234ze refrigerant for different evaporators loads ($Q_{eva1} = 35$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$) at was obtained at evaporators of different temperatures ($T_{eva1} = 268$ K, $T_{eva2} = 278$ K, and $T_{eva3} = 283$ K) shown in Table-2(f). Similarly, the exergy efficiency of VCR systems using multiple evaporator compressors of individual types with expansion valves for numerous kinds using HFO-1234ze refrigerant for different evaporators loads ($Q_{eva1} = 105$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 35$) at was obtained at evaporators of different temperatures ($T_{eva1} = 263$ K, $T_{eva2} = 273$ K, and $T_{eva3} = 278$ K) respectively.

Table-1(b) Different evaporators Load conditions used in VCRS using HFO-1234ze refrigerant using multiple evaporators at different temperatures with compressors of individual types and expansion valves of multiple types

| S.N | Evaporator load Parameters | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|-----|--|--------|---------|----------|---------|--------|---------|
| 1 | First Evaporator Load (Q_{Eva1}) “kW” | 105 | 105 | 70 | 70 | 35 | 35 |
| 2 | Second Evaporator Load (Q_{Eva2}) “kW” | 70 | 35 | 105 | 35 | 70 | 105 |
| 3 | Third Evaporator Load (Q_{Eva3}) “kW” | 35 | 70 | 35 | 105 | 105 | 70 |

Table-1(c) Different evaporators load conditions used in VCRS using HFO-1234ze refrigerant using multiple evaporators at different temperatures with compressors of individual types and expansion valves of multiple types

| S.N | Evaporator Temperature Parameters | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|-----|---|--------|---------|----------|---------|--------|---------|
| 1 | First Evaporator temperature (T_{Eva1}) “K” | 263 | 263 | 263 | 268 | 268 | 268 |
| 2 | Second Evaporator temperature (T_{Eva2}) “kW” | 273 | 273 | 278 | 273 | 273 | 278 |
| 3 | Third Evaporator temperature (T_{Eva3}) “kW” | 278 | 283 | 283 | 278 | 283 | 283 |

Table2(a): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$, compressors isentropic efficiency= 100%)

| Performance Parameters using R1234ze in given table-1(b) | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| First law Efficiency (COP _{VCRS}) | 5.601 | 5.715 | 5.851 | 6.105 | 6.402 | 6.26 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.114 | 1.123 | 1.185 | 1.215 | 1.306 | 1.286 |
| Exergetic Efficiency | 0.4973 | 0.4893 | 0.4805 | 0.4628 | 0.4427 | 0.4526 |
| Exergy of Fuel “kW” | 37.49 | 36.75 | 35.89 | 34.4 | 32.8 | 33.55 |
| Exergy of product “kW” | 18.64 | 17.98 | 17.24 | 15.92 | 14.52 | 15.8 |
| First compressor Work “kW” | 18.06 | 18.06 | 12.04 | 12.04 | 6.02 | 6.02 |
| Second compressor Work “kW” | 9.792 | 5.16 | 14.25 | 4.984 | 9.44 | 14.07 |
| Third compressor Work “kW” | 9.641 | 13.53 | 9.604 | 17.38 | 17.34 | 13.45 |

Table -2(b): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze in given table-1(b) | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 5.821 | 6.072 | 6.09 | 6.667 | 7.023 | 6.689 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.077 | 1.133 | 1.142 | 1.285 | 1.393 | 1.297 |
| Exergy Efficiency | 0.4991 | 0.4829 | 0.4816 | 0.4444 | 0.4214 | 0.4428 |
| Exergy of Fuel “kW” | 36.08 | 34.59 | 34.48 | 31.5 | 29.9 | 31.39 |
| Exergy of product “kW” | 18.0 | 16.7 | 16.61 | 14.0 | 12.6 | 13.9 |
| First compressor Work “kW” | 18.06 | 18.06 | 12.04 | 12.04 | 6.02 | 6.02 |
| Second compressor Work “kW” | 10.73 | 5.918 | 15.18 | 5.551 | 10.0 | 14.82 |
| Third compressor Work “kW” | 7.283 | 10.61 | 7.257 | 13.91 | 13.88 | 10.56 |

Table 2(c): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze in given table-1(b) | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 6.064 | 6.193 | 6.516 | 6.826 | 7.397 | 7.214 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.130 | 1.152 | 1.259 | 1.324 | 1.527 | 1.476 |
| Exergetic Efficiency | 0.4817 | 0.4730 | 0.4535 | 0.4331 | 0.3971 | 0.4093 |
| Exergy of Fuel “kW” | 34.63 | 33.91 | 32.23 | 30.79 | 28.39 | 29.11 |
| Exergy of product “kW” | 16.68 | 16.04 | 14.62 | 13.34 | 11.27 | 11.91 |
| First compressor Work “kW” | 18.77 | 18.77 | 12.51 | 12.51 | 6.257 | 6.257 |
| Second compressor Work “kW” | 8.598 | 4.541 | 12.49 | 4.38 | 8.275 | 12.33 |
| Third compressor Work “kW” | 7.259 | 10.6 | 7.22 | 13.9 | 13.86 | 10.52 |

Table -2(d): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva3}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 5.999 | 6.13 | 6.134 | 6.414 | 6.565 | 6.419 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.235 | 1.251 | 1.275 | 1.314 | 1.364 | 1.341 |
| Exergetic Efficiency | 0.4716 | 0.4625 | 0.4621 | 0.4427 | 0.4318 | 0.4423 |

| | | | | | | |
|-----------------------------|-------|-------|-------|-------|-------|-------|
| Exergy of Fuel “kW” | 35.0 | 34.26 | 34.23 | 32.74 | 31.97 | 32.72 |
| Exergy of product“kW” | 16.51 | 15.84 | 15.82 | 14.49 | 1381 | 14.47 |
| First compressor Work “kW” | 15.64 | 15.64 | 10.43 | 10.43 | 5.213 | 5.213 |
| Second compressor Work “kW” | 9.782 | 5.15 | 14.24 | 4.977 | 9.437 | 14.07 |
| Third compressor Work “kW” | 9.584 | 13.47 | 9.566 | 17.34 | 17.32 | 13.43 |

Table -2(e): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=268K, T_{eva2}=273K, T_{eva3}=283K, T_{Cond}=313K, T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 6.251 | 6.541 | 6.397 | 7.036 | 7.222 | 6.87 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.20 | 1.274 | 1.233 | 1.412 | 1.466 | 1.358 |
| Exergetic Efficiency | 0.4723 | 0.4536 | 0.4624 | 0.4213 | 0.4088 | 0.4315 |
| Exergy of Fuel “kW” | 33.6 | 32.11 | 32.83 | 29.85 | 29.08 | 30.57 |
| Exergy of product“kW” | 15.87 | 14.56 | 15.18 | 12.57 | 11.89 | 13.19 |
| First compressor Work “kW” | 15.64 | 15.64 | 10.43 | 10.43 | 5.213 | 5.213 |
| Second compressor Work “kW” | 10.71 | 5.897 | 15.17 | 5.537 | 9.993 | 14.81 |
| Third compressor Work “kW” | 7.244 | 10.57 | 7.231 | 13.88 | 13.87 | 10.54 |

Table -2(f): Ideal thermal performances of VCR systems using multiple evaporator & compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant using ($T_{eva1}=268K, T_{eva2}=278K, T_{eva3}=283K, T_{Cond}=313K, T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 6.552 | 6.702 | 6.883 | 7.223 | 7.628 | 7.434 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.265 | 1.296 | 1.372 | 1.457 | 1.616 | 1.556 |
| Exergetic Efficiency | 0.4537 | 0.4437 | 0.4324 | 0.4097 | 0.3836 | 0.3965 |
| Exergy of Fuel “kW” | 32.05 | 31.33 | 30.51 | 29.07 | 27.53 | 28.25 |
| Exergy of product“kW” | 14.54 | 13.19 | 13.19 | 11.91 | 10.56 | 11.2 |
| First compressor Work “kW” | 16.24 | 16.24 | 10.83 | 10.83 | 5.415 | 5.415 |
| Second compressor Work “kW” | 8.588 | 4.532 | 12.49 | 4.373 | 8.272 | 12.33 |
| Third compressor Work “kW” | 7.218 | 10.56 | 7.193 | 13.87 | 13.84 | 10.51 |

Exergy destruction in components of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions are shown in Table-3(a) to Table-3(f), respectively. It was found that the VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions of $Q_{eva1}=35$ kW, $Q_{eva2}=70$ kW, $Q_{eva3}=105$ kW gives maximum

exergy destruction in compressor with lowest in throttle expansion valves at $Q_{eva1}=105$ kW, $Q_{eva2}=70$ kW, $Q_{eva3}=35$ kW. Similarly, minimum total exergy destruction (%) with maximum rational exergy efficiency was found in different load conditions of $Q_{eva1}=105$ kW, $Q_{eva2}=35$ kW, $Q_{eva3}=70$ kW at evaporators of different temperatures ($T_{eva1}=263$ K, $T_{eva2}=273$ K, and $T_{eva3}=283$ K) respectively.

Table -3(a): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K, T_{eva2}=273K, T_{eva3}=278K, T_{Cond}=313K, T_{Subcooled_Liquid}=303K$, compressors isentropic efficiency= 100%)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 28.96 | 29.46 | 30.06 | 31.17 | 32.48 | 31.86 |
| Evaporator | 18.36 | 17.36 | 18.68 | 16.55 | 16.81 | 17.94 |
| Expansion Valves | 8.048 | 8.135 | 8.177 | 8.369 | 8.526 | 8.419 |
| Total Exergy Destruction | 55.38 | 54.96 | 56.92 | 56.10 | 57.82 | 58.21 |
| Rational Efficiency | 44.62 | 45.08 | 43.08 | 43.90 | 42.18 | 41.79 |

Table -3(b): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K, T_{eva2}=273K, T_{eva3}=283K, T_{Cond}=313K, T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 29.3 | 31.03 | 31.11 | 33.64 | 35.2 | 33.74 |
| Evaporator | 17.39 | 17.17 | 17.34 | 16.85 | 16.76 | 17.04 |
| Expansion Valves | 6.451 | 6.50 | 6.522 | 6.635 | 6.727 | 6.660 |
| Total Exergy Destruction | 53.77 | 54.7 | 54.98 | 57.13 | 58.69 | 57.44 |

Table 3(c): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 31.0 | 31.56 | 32.98 | 34.32 | 36.85 | 36.05 |
| Evaporator | 16.74 | 16.18 | 17.43 | 16.23 | 16.97 | 17.62 |
| Expansion Valves | 6.679 | 6.743 | 6.671 | 6.814 | 6.817 | 6.738 |
| Total Exergy Destruction | 54.42 | 54.48 | 57.09 | 57.36 | 60.64 | 60.41 |
| Rational Efficiency | 45.58 | 45.52 | 42.91 | 42.64 | 39.36 | 39.59 |

Table 3(d): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva2}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 30.71 | 31.28 | 31.3 | 32.53 | 33.21 | 32.55 |
| Evaporator | 19.38 | 18.37 | 19.39 | 17.19 | 17.14 | 18.29 |
| Expansion Valves | 8.145 | 8.241 | 8.249 | 8.455 | 8.574 | 8.463 |
| Total Exergy Destruction | 58.24 | 57.86 | 58.94 | 58.17 | 58.92 | 59.31 |
| Rational Efficiency | 41.76 | 42.14 | 41.06 | 41.83 | 41.08 | 40.69 |

Table 3(e): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva2}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 31.82 | 33.09 | 32.46 | 35.26 | 36.08 | 34.53 |
| Evaporator | 18.39 | 18.2 | 18.02 | 17.57 | 17.1 | 17.39 |
| Expansion Valves | 6.452 | 6.502 | 6.524 | 6.646 | 6.735 | 6.666 |
| Total Exergy Destruction | 56.6 | 57.79 | 57.0 | 59.48 | 59.94 | 58.59 |
| Rational Efficiency | 43.34 | 42.21 | 43.0 | 40.52 | 40.06 | 41.41 |

Table 3(f): Ideal Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva2}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$,

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Condenser | 33.14 | 33.8 | 34.59 | 36.09 | 37.86 | 37.01 |
| Evaporator | 17.81 | 17.22 | 18.22 | 16.98 | 17.4 | 18.05 |
| Expansion Valves | 6.426 | 6.491 | 6.494 | 6.636 | 6.723 | 6.645 |
| Total Exergy Destruction | 57.37 | 57.51 | 59.31 | 59.71 | 61.98 | 61.71 |
| Rational Efficiency | 42.63 | 42.49 | 40.69 | 40.29 | 38.02 | 38.29 |

Actual thermal performances of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions are shown in Table-4(a) to Table-4(f), respectively. It was found that the VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions of $Q_{eva1} = 35$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$ kW give maximum first law efficiency in terms of coefficient of performance(COP) with lowest electrical energy consumption in terms of total compressors work for running whole system. In contrast, maximum exergy efficiency was found in different load conditions of $Q_{eva1} = 105$ kW, $Q_{eva2} = 70$ kW, and $Q_{eva3} = 35$ kW with maximum electrical energy consumption in terms of total compressors work for running the whole system. However best first law efficiency (COP) of VCR systems using multiple evaporator compressors of individual types with expansion

valves of various types using HFO-1234ze refrigerant for different evaporators loads ($Q_{eva1} = 35$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$) at was obtained at evaporators of different temperatures ($T_{eva1} = 268$ K, $T_{eva2} = 278$ K, and $T_{eva3} = 283$ K) shown in Table-2(f). Similarly, the exergy efficiency of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different evaporators loads ($Q_{eva1} = 105$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 35$) at was obtained at evaporators of different temperatures ($T_{eva1} = 263$ K, $T_{eva2} = 273$ K, and $T_{eva3} = 278$ K) respectively.

Table -4(a): Actual thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze in given table-1(b) | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.201 | 4.286 | 4.388 | 4.578 | 4.802 | 4.695 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.784 | 1.804 | 1.878 | 1.933 | 2.059 | 2.023 |
| Exergetic Efficiency | 0.373 | 0.3670 | 0.3604 | 0.3471 | 0.3320 | 0.3394 |
| Exergy of Fuel “kW” | 49.99 | 49.0 | 47.86 | 45.87 | 43.73 | 44.73 |
| Exergy of product“kW” | 18.64 | 17.98 | 17.24 | 15.92 | 14.52 | 15.8 |
| First compressor Work “kW” | 24.28 | 24.28 | 16.05 | 16.05 | 8.026 | 8.026 |
| Second compressor Work “kW” | 13.06 | 6.88 | 19.0 | 6.645 | 12.59 | 18.76 |
| Third compressor Work “kW” | 12.85 | 18.04 | 12.81 | 23.17 | 23.12 | 17.94 |

Table 4(b): Actual thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze in given table-1(b) | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.366 | 4.554 | 4.568 | 5.0 | 5.267 | 5.017 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.745 | 1.823 | 1.834 | 2.035 | 2.184 | 2.05 |
| Exergetic Efficiency | 0.3743 | 0.3622 | 0.3612 | 0.3333 | 0.3160 | 0.3321 |
| Exergy of Fuel “kW” | 48.1 | 46.11 | 45.97 | 42.0 | 39.87 | 41.86 |
| Exergy of product“kW” | 18.0 | 16.7 | 16.61 | 14.0 | 12.6 | 13.9 |
| First compressor Work “kW” | 24.08 | 24.08 | 16.05 | 16.05 | 8.026 | 8.026 |
| Second compressor Work “kW” | 14.31 | 7.891 | 20.24 | 7.401 | 13.33 | 19.76 |
| Third compressor Work “kW” | 9.71 | 14.14 | 9.676 | 18.54 | 18.51 | 14.08 |

Table -4(c): Actual thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva3}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.548 | 4.645 | 4.887 | 5.115 | 5.548 | 5.411 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.822 | 1.857 | 1.994 | 2.094 | 2.366 | 2.29 |
| Exergetic Efficiency | 0.3612 | 0.3547 | 0.3401 | 0.3249 | 0.2978 | 0.3070 |
| Exergy of Fuel “kW” | 46.17 | 45.21 | 42.97 | 41.05 | 37.85 | 38.81 |
| Exergy of product“kW” | 16.68 | 16.04 | 14.62 | 13.34 | 11.27 | 11.91 |
| First compressor Work “kW” | 25.03 | 25.03 | 16.69 | 16.69 | 8.343 | 8.343 |
| Second compressor Work “kW” | 11.46 | 6.055 | 16.66 | 5.840 | 11.03 | 16.44 |
| Third compressor Work “kW” | 9.678 | 14.13 | 9.628 | 18.53 | 18.48 | 14.03 |

Table -4(d): Actual thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva3}=273K$, $T_{eva3}=278K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.499 | 4.597 | 4.601 | 4.81 | 4.926 | 4.814 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.942 | 1.972 | 1.997 | 2.067 | 2.136 | 2.095 |
| Exergetic Efficiency | 0.3537 | 0.3468 | 0.3466 | 0.3320 | 0.3239 | 0.3317 |
| Exergy of Fuel “kW” | 46.67 | 45.68 | 45.64 | 43.66 | 42.63 | 43.62 |
| Exergy of product“kW” | 16.51 | 15.84 | 15.82 | 14.49 | 13.81 | 14.47 |
| First compressor Work “kW” | 20.85 | 20.85 | 13.9 | 13.9 | 6.951 | 6.951 |
| Second compressor Work “kW” | 13.04 | 6.866 | 18.99 | 6.636 | 12.51 | 18.76 |
| Third compressor Work “kW” | 12.78 | 17.96 | 12.75 | 23.12 | 23.1 | 17.91 |

Table -4(e): Actual Thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva3}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.688 | 4.906 | 4.798 | 5.277 | 5.417 | 5.153 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.905 | 2.009 | 1.954 | 2.203 | 2.282 | 2.13 |
| Exergetic Efficiency | 0.3542 | 0.3402 | 0.3468 | 0.3160 | 0.3066 | 0.3236 |
| Exergy of Fuel “kW” | 44.79 | 42.81 | 43.77 | 39.79 | 38.77 | 40.76 |
| Exergy of product“kW” | 15.87 | 14.56 | 15.18 | 12.57 | 11.89 | 13.19 |
| First compressor Work “kW” | 20.85 | 20.85 | 13.9 | 13.9 | 6.951 | 6.951 |
| Second compressor Work “kW” | 14.28 | 7.863 | 20.23 | 7.382 | 13.32 | 19.75 |

Table -4(f): Actual Thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| Performance Parameters using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| COP _{VCRS} | 4.914 | 5.027 | 5.162 | 5.418 | 5.721 | 5.575 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.999 | 2.048 | 2.143 | 2.271 | 2.485 | 2.397 |
| Exergetic Efficiency | 0.3403 | 0.3328 | 0.3243 | 0.3073 | 0.2877 | 0.2974 |
| Exergy of Fuel “kW” | 42.73 | 41.78 | 40.68 | 38.76 | 36.71 | 37.67 |
| Exergy of product “kW” | 14.54 | 13.19 | 13.19 | 11.91 | 10.56 | 11.2 |
| First compressor Work “kW” | 21.66 | 21.66 | 14.44 | 14.44 | 7.219 | 7.219 |
| Second compressor Work “kW” | 11.45 | 6.042 | 16.65 | 5.831 | 11.03 | 16.44 |
| Third compressor Work “kW” | 9.624 | 1408 | 9.59 | 18.49 | 18.46 | 14.01 |

Actual exergy destruction (%) in each component of VCR systems was computed at 75% compressors efficiencies using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions are shown in Table-5(a) to Table-5(f) respectively. It was found that the VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions of Q_{eva1}

=35 kW, Q_{eva2}=70 kW, Q_{eva3} =105 kW gives maximum exergy destruction in compressor with lowest in throttle expansion valves at Q_{eva1}=105 kW, Q_{eva2}=70 kW, Q_{eva3}=35 kW. Similarly, minimum total exergy destruction (%) with maximum rational exergy efficiency was found in different load conditions of Q_{eva1}=105 kW, Q_{eva2}=35 kW, Q_{eva3}=70 kW at evaporators of different temperatures (T_{eva1}= 263 K, T_{eva2}= 273 K, and T_{eva3}=283 K) respectively.

Table -5(a): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva2}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.67 | 23.67 | 23.68 | 23.68 | 23.7 | 23.69 |
| Condenser | 23.06 | 23.43 | 23.87 | 24.7 | 25.66 | 25.2 |
| Evaporator | 13.77 | 13.02 | 14.01 | 12.42 | 12.61 | 13.45 |
| Expansion Valves | 6.036 | 6.102 | 6.133 | 6.277 | 6.394 | 6.315 |
| Total Exergy Destruction | 66.53 | 66.22 | 67.69 | 67.07 | 68.36 | 68.66 |
| Rational Efficiency | 33.47 | 33.78 | 32.31 | 32.93 | 31.64 | 31.34 |

Table -5(b): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva2}=273K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.67 | 23.67 | 23.68 | 23.69 | 23.7 | 23.7 |
| Condenser | 23.78 | 24.6 | 24.65 | 26.54 | 27.7 | 26.61 |
| Evaporator | 13.05 | 12.88 | 13.01 | 12.64 | 12.57 | 12.78 |
| Expansion Valves | 4.838 | 4.875 | 4.892 | 4.976 | 5.045 | 4.995 |
| Total Exergy Destruction | 65.33 | 66.03 | 66.23 | 67.85 | 69.02 | 68.08 |
| Rational Efficiency | 34.67 | 33.97 | 33.77 | 32.15 | 30.98 | 31.92 |
| Second law efficiency(%) | 58.1 | 60.60 | 60.79 | 66.54 | 70.09 | 66.77 |

Table -5(c): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.67 | 23.67 | 23.69 | 23.69 | 23.71 | 23.71 |
| Condenser | 24.58 | 25.0 | 26.05 | 27.05 | 28.92 | 28.33 |
| Evaporator | 12.15 | 12.13 | 13.08 | 12.17 | 12.73 | 13.22 |
| Expansion Valves | 5.009 | 5.057 | 5.004 | 5.11 | 5.113 | 5.054 |
| Total Exergy Destruction | 65.81 | 65.86 | 67.81 | 68.02 | 70.48 | 70.31 |
| Rational Efficiency | 34.19 | 34.14 | 32.19 | 31.98 | 29.52 | 29.69 |

Table -5(d): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K, T_{eva3}=273K, T_{eva3}=278K, T_{Cond}=313K, T_{Subcooled_Liquid}=303K$)

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.69 | 23.69 | 23.69 | 23.70 | 23.70 | 23.70 |
| Condenser | 24.35 | 24.77 | 24.79 | 25.7 | 26.2 | 25.71 |
| Evaporator | 14.54 | 13.75 | 14.54 | 12.89 | 12.86 | 13.72 |
| Expansion Valves | 6.109 | 6.181 | 6.187 | 6.341 | 6.43 | 6.348 |
| Total Exergy Destruction | 68.68 | 68.39 | 69.20 | 68.63 | 69.19 | 69.48 |
| Rational Efficiency | 31.32 | 31.61 | 30.80 | 31.37 | 30.81 | 30.52 |
| Second Law efficiency (%) | 50.37 | 51.46 | 51.50 | 53.85 | 55.15 | 53.89 |

Table -5(e): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K, T_{eva3}=273K, T_{eva3}=283K, T_{Cond}=313K$,

| % Exergy Destruction in components using R1234ze | Case-I | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.69 | 23.69 | 23.7 | 23.7 | 23.71 | 23.71 |
| Condenser | 25.17 | 26.12 | 25.65 | 27.74 | 28.35 | 27.19 |
| Evaporator | 13.79 | 13.65 | 13.51 | 13.18 | 12.84 | 13.04 |
| Expansion Valves | 4.839 | 4.878 | 4.895 | 4.984 | 5.051 | 5.0 |
| Total Exergy Destruction | 67.49 | 68.34 | 67.75 | 69.61 | 69.96 | 68.94 |
| Rational Efficiency | 32.51 | 31.66 | 32.25 | 30.39 | 30.04 | 31.04 |
| Second Law Efficiency (%) | 0.5248 | 0.5492 | 0.5371 | 0.5907 | 0.6060 | 0.5768 |

Table -5(f): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO-1234ze refrigerant using ($T_{eva1}=268K, T_{eva3}=273K, T_{eva3}=283K, T_{Cond}=313K$,

| % Exergy Destruction in components using R1234ze | Case-1 | Case-II | Case-III | Case-IV | Case-V | Case-VI |
|--|--------|---------|----------|---------|--------|---------|
| Compressor | 23.7 | 23.7 | 23.71 | 23.71 | 23.72 | 23.72 |
| Condenser | 26.16 | 26.65 | 27.24 | 28.35 | 29.67 | 29.04 |
| Evaporator | 13.36 | 12.92 | 13.67 | 12.74 | 13.05 | 13.54 |
| Expansion Valves | 4.82 | 4.868 | 4.871 | 4.977 | 5.043 | 4.963 |
| Total Exergy Destruction | 68.03 | 68.14 | 69.48 | 69.78 | 71.48 | 71.28 |
| Rational Efficiency | 31.97 | 31.86 | 30.52 | 30.22 | 28.52 | 28.72 |

2.1 Effect of different low GWP environmental friendly refrigerants used in of VCR systems

Actual thermal performances of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions are shown in Table-6(a) to Table-6(c), respectively. It was found that the VCR systems using

multiple evaporator compressors of individual types with expansion valves of various types using HFO-1233zd(E) refrigerant give maximum first-law efficiency in terms of coefficient of performance(COP) with the lowest electrical energy consumption in terms of total compressors work for running the whole system. The maximum was found using R32 refrigerant.

Table-6(a): Actual thermal performances of multiple evaporator compressors of individual expansion valves of VCR systems using ($T_{eva1}=263K, T_{eva3}=278K, T_{eva3}=283K, T_{Cond}=313K, Q_{eva1} = 70 \text{ "kW"}, Q_{eva2} = 105 \text{ "kW"}, Q_{eva3} = 35 \text{ "kW"}$ at compressors efficiencies of 75%

| Performance Parameters using | R1234ze | R1234yf | R152a | R245fa | R-32 | R12 |
|--|---------|---------|--------|--------|--------|--------|
| COP _{VCRS} | 4.887 | 4.767 | 4.893 | 4.986 | 4.588 | 4.864 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.994 | 2.066 | 1.978 | 1.938 | 2.153 | 1.954 |
| Exergetic Efficiency | 0.3402 | 0.3318 | 0.3405 | 0.3405 | 0.3193 | 0.3385 |
| Exergy of Fuel "kW" | 42.97 | 44.05 | 42.92 | 42.12 | 45.77 | 43.17 |
| Exergy of product "kW" | 14.62 | 14.62 | 14.62 | 14.62 | 14.62 | 14.62 |

Table-6(b): Actual Thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using using ($T_{eva1}=263K, T_{eva3}=278K, T_{eva3}=283K, T_{Cond}=313K, Q_{eva1} = 70 \text{ "kW"}, Q_{eva2} = 105 \text{ "kW"}, Q_{eva3} = 35 \text{ "kW"}$ at compressors efficiencies of 75%

| Performance Parameters | R1233 zd(E) | R1336 mzz(Z) | R1225 ye(Z) | R1243 zf | R-1224 yd(Z) |
|--|-------------|--------------|-------------|----------|--------------|
| COP _{VCRS} | 4.987 | 4.966 | 4.841 | 4.756 | 4.97 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 1.936 | 1.956 | 2.02 | 2.072 | 1.947 |
| Exergetic Efficiency | 0.3471 | 0.340 | 0.3369 | 0.3310 | 0.3459 |
| Exergy of Fuel "kW" | 42.11 | 42.29 | 43.38 | 44.15 | 42.26 |
| Exergy of product "kW" | 14.62 | 14.62 | 14.62 | 14.62 | 14.62 |

Table-6(c): Actual Thermal performances of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO & HFC blends (refrigerants) using ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $Q_{eva1} = 70$ “kW”, $Q_{eva2} = 105$ “kW” $Q_{eva3} = 35$ “kW” at compressors efficiencies of 75%)

| Performance Parameters | R513a | R515a | R454b | R452a | R450a |
|--|--------|--------|--------|--------|-------|
| COP _{VCRS} | 4.788 | 4.843 | 4.455 | 4.293 | 4.712 |
| Exergy Destruction Ratio(EDR _{VCRS}) | 2.05 | 2.017 | 2.246 | 2.415 | 2.109 |
| Exergetic Efficiency | 0.3333 | 0.3371 | 0.3101 | 0.2988 | 0.328 |
| Exergy of Fuel “kW” | 43.8 | 43.36 | 47.14 | 48.91 | 44.57 |
| Exergy of product“kW” | 14.62 | 14.62 | 14.62 | 14.62 | 14.62 |

Exergy destruction (%) in Each component of VCR systems using multiple evaporator compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant for different load conditions are shown in Table-7(a) to Table-7(c) respectively. It was found that the VCR systems using multiple evaporator compressors of individual

types with expansion valves of multiple types using HFC-32 refrigerant give maximum exergy destruction in condenser with lowest in throttle expansion valves. Similarly, minimum total exergy destruction (%) with maximum rational exergy efficiency was found using HCFO-1233zd(E).

Table-7(a): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFOs & HFCs refrigerants and comparison with CFC-12 for ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $Q_{eva1} = 70$ “kW”, $Q_{eva2} = 105$ “kW” $Q_{eva3} = 35$ “kW” at compressors efficiencies of 75%)

| Exergy Destruction in components R1234ze | R1234ze | R1234yf | R152a | R245fa | R-32 | R12 |
|--|---------|---------|-------|--------|-------|-------|
| Compressor (%) | 23.69 | 23.73 | 22.58 | 23.64 | 23.52 | 23.05 |
| Condenser (%) | 26.05 | 25.07 | 28.31 | 26.75 | 30.80 | 27.12 |
| Evaporator (%) | 13.08 | 13.69 | 12.59 | 13.16 | 11.85 | 12.80 |
| Expansion Valves (%) | 5.003 | 6.082 | 3.877 | 3.719 | 4.796 | 4.544 |
| Total Exergy Destruction (%) | 67.81 | 68.56 | 67.35 | 67.27 | 68.77 | 67.52 |
| Rational Efficiency(%) | 32.19 | 31.44 | 32.65 | 32.63 | 31.23 | 32.48 |
| Irreversibility Ratio (I.R) | 2.106 | 2.18 | 2.063 | 2.062 | 2.202 | 2.079 |

Table-7(b): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO refrigerants using ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $Q_{eva1} = 70$ “kW” $Q_{eva2} = 105$ “kW” $Q_{eva3} = 35$ “kW” at compressors efficiencies of 75%)

| % Exergy Destruction in components | R1233 zd(E) | R1336 mzz(Z) | R1225 ye(Z) | R1243 zf | R-1224 yd(Z) |
|------------------------------------|-------------|--------------|-------------|----------|--------------|
| Compressor | 23.52 | 23.80 | 23.64 | 23.38 | 23.68 |
| Condenser | 27.18 | 26.55 | 25.79 | 25.7 | 26.8 |
| Evaporator | 13.01 | 13.37 | 13.44 | 14.34 | 13.14 |
| Expansion Valves | 3.469 | 3.896 | 5.205 | 5.177 | 3.734 |
| Total Exergy Destruction | 67.17 | 67.62 | 68.08 | 68.59 | 67.36 |
| Rational Efficiency | 32.81 | 32.38 | 31.92 | 31.41 | 32.64 |

Table-7(c): Actual Exergy Destruction (%) in Each components of multiple evaporator compressors of individual types expansion valves of multiple types of VCR systems using HFO+HFC blended refrigerants using HFO & HFC blends (refrigerants) using ($T_{eva1}=263K$, $T_{eva2}=278K$, $T_{eva3}=283K$, $T_{Cond}=313K$, $Q_{eva1} = 70$ “kW”, $Q_{eva2} = 105$ “kW” $Q_{eva3} = 35$ “kW” at compressors efficiencies of 75%)

| % Exergy Destruction in components | R513a | R515a | R454b | R452a | R450a |
|------------------------------------|-------|-------|-------|-------|-------|
| Compressor | 23.52 | 23.66 | 21.79 | 23.64 | 22.9 |
| Condenser | 25.68 | 26.79 | 31.29 | 25.27 | 25.68 |
| Evaporator | 13.38 | 12.74 | 11.5 | 17.0 | 14.82 |
| Expansion Valves | 5.72 | 4.798 | 5.062 | 6.998 | 5.256 |
| Total Exergy Destruction | 68.3 | 67.99 | 69.64 | 72.17 | 69.15 |
| Rational Efficiency | 31.7 | 32.01 | 30.36 | 27.83 | 30.85 |

3. Conclusions

Follow conclusions were drawn

- (i) The best first law efficiency (COP) of VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different evaporators loads ($Q_{eva1} = 35$

kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$) at evaporators of different temperatures ($T_{eva1} = 268$ K, $T_{eva2} = 278$ K, and $T_{eva3} = 283$ K) was found.

- (ii) Actual thermodynamic performances of VCRS systems at 75% of all compressors efficiencies using multiple evaporator compressors of individual types with expansion valves of multiple types using HFO-1234ze refrigerant for different load conditions are given

- maximum COP with lowest electrical energy consumption in terms of total compressors work for running the whole system. The maximum was found using R32 refrigerant.
- (iii) The VCR systems using multiple evaporator compressors of individual types with expansion valves of various types using HFC-32 refrigerant give maximum exergy destruction in condenser with lowest in throttle expansion valves.
 - (iv) Minimum total exergy destruction (%) in VCR system with maximum rational exergy efficiency was found by using ultra-low GWP HCFO-1233zd(E) refrigerant.
 - (v) Exergy destruction computation in each component of VCR systems using multiple evaporators, compressors of individual types with expansion valves of various types using HFO-1234ze refrigerant for different load conditions (of $Q_{eva1} = 35$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 105$) gives maximum exergy destruction in compressor with lowest in throttle expansion valves (at $Q_{eva1} = 105$ kW, $Q_{eva2} = 70$ kW, $Q_{eva3} = 35$ kW).
 - (vi) The minimum total exergy destruction (%) in the VCR system with maximum rational exergy efficiency was found at different load conditions of $Q_{eva1} = 105$ kW, $Q_{eva2} = 35$ kW, $Q_{eva3} = 70$ kW at evaporators of different temperatures ($T_{eva1} = 263$ K, $T_{eva2} = 273$ K, and $T_{eva3} = 283$ K) respectively.

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