



ORIGINAL ARTICLE

Thermodynamic static and dynamic performances of VCERS using low GWP blends of HFC+HFO refrigerants in higher temperature cycle using blends of HFC+HFO refrigerants in low GWP refrigerant in low temperature cycle

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Abstract

In this paper, comparison of static and dynamic thermodynamic energy-exergy performances of eight optimal combinations of cascaded vapor compression refrigeration system for the ultra-low applications using ecofriendly low global warming potential GWP blends of HFC+HFO refrigerants in higher temperature cycle in the temperature range of 50° C to -30° C and also using blends of HFC+HFO refrigerants in low GWP in low temperature cycle between (-30° C to -70° C) have been analyzed. It was found that the optimal Cascaded vapor compression refrigeration system 44 using ecofriendly low GWP R452B refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle gives best (optimum) thermodynamic first law energy performance (COP) and second law (exergetic efficiency) performances with lowest electrical energy consumption. in the dynamic performances it was found that by increasing temperature overlapping, decreases the thermodynamic performances of cascaded refrigeration systems.

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1. Introduction

In current decades many countries have been taken more consideration to environmental pollution caused by CFCs. Burning fossil fuels because vapor compression refrigeration system based applications make use of refrigerants which are responsible for greenhouse gases, global warming and ozone layer depletion. Montreal protocol was signed on the issue of substances that are responsible for depleting Ozone layer and discovered how much consumption and production of ozone depletion substances took place during certain time period for both developed and developing countries. Another protocol named as Kyoto aimed to control emission of greenhouse gases in 1997. The relationship between ozone depletion potential and global warming potential is the major concern in the field

of GRT (green refrigeration technology) so Kyoto proposed new refrigerants having lower value of ODP and GWP. Internationally a program being pursued to phase out refrigerants having high chlorine content for the sake of global environmental problems. Due to presence of high chlorine content, high global warming potential and ozone depletion potential after 90's CFC and HCFC refrigerants have been restricted. Thus, HFC refrigerants are used nowadays, showing much lower global warming potential value, but still high with respect to non-fluorine refrigerants. Lots of research work has been done for replacing "old" refrigerants with "new" refrigerants [1]. The thermodynamic performances of systems based on vapor compression refrigeration technology can be improved by following methods.

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The performance of refrigerator is evaluated in term of COP which is the ratio of refrigeration effect to the net work input given to the system. The COP of vapor compression refrigeration system (VCRS) can be improved either by increasing refrigeration effect or by reducing work input given to the system.

We know that the throttling process in VCR is an irreversible expansion process. The expansion process is one of the main factors responsible for exergy loss in cycle performance because of entering the portion of the refrigerant flashing to vapor in the evaporator which will not only reduce the cooling capacity but also increase the size of the evaporator. This problem can be eliminated by adopting multi-stage expansion with a flash chamber where the flash vapors are removed after each stage of expansion as a consequence there will be an increase in cooling capacity and reduce the size of the evaporator. The compressor work (input electrical energy consumption) can also be reduced by replacing multi-stage compression or compound compression with single-stage compression. Similarly, the refrigeration effect can also be increased by passing the refrigerant through the sub-cooler after the condenser to the evaporator [2-3]. Nikolaidis and Probert [4] studied analytically that change in evaporator and condenser temperatures of two-stage vapor compression refrigeration plant using R22 add considerable effect on plant irreversibility. They suggested that there is a need for optimizing the conditions imposed upon the condenser and evaporator. Getu and Bansal [5] had optimized the design and operating parameters of condensing temperature, subcooling temperature, evaporating temperature, superheating temperature, and temperature difference in cascade heat exchanger R744-R717 cascade refrigeration system. A regression analysis was also done to obtain optimum thermodynamic parameters of the same system. Mishra [5] described thermodynamic analysis of cascade refrigeration system with huge refrigerant sinking CFC, HCFC, HFC, HFO, and HFO refrigerants, etc., and optimizations conducted for such refrigerants. A huge number of refrigerants have been examined in a cascade system for determining the appropriate combination of refrigerants in high temperature and low-temperature cycle circuits of refrigerants however the trends show that the HFO refrigerants a natural refrigerant is gaining more importance due to environmental conditions few natural refrigerants. [3].

Exergy analysis is a useful way for determining the real thermodynamic losses and optimizing environmental and economic performance in the systems such as vapor compression refrigeration systems. Alptunganbaba et.al.[7] carried out exergy analysis of a two evaporator vapor compression refrigeration system using R1234yf, R1234ze, and R134a as refrigerants and computed the effect of evaporator and condenser temperatures on the exergy destruction and exergy efficiency of the system Adrián Mota-Babiloni [8] studied the feasibility of R454C and R455A, refrigerants, in vapor compression refrigeration systems as alternatives to R404A and found that the R454C and R455A

will be the most viable low GWP options to perform a direct replacement of R404A. This paper mainly deals with the static and dynamic thermodynamic energy & exergy performances of eight optimal cascaded vapor compression using HFO+HFC blends.

2. Results and Discussion

In this paper, two types of thermodynamic energy and exergy performances for different optimal combination of cascaded vapor compression refrigeration systems have been computed. The numerical computation was carried out for optimal conditions explained in details. However dynamic thermodynamic performances have been computed with varying HTC evaporator temperature from -0°C to -30°C , the HTC condenser temperature variation from 40°C to 60°C , LTC evaporator temperature from -50°C to -70°C and temperature overlapping from 0°C to 15°C .

2.1 Static thermodynamic performances

For finding static thermodynamic (energy and exergetic) performances of cascaded vapor compression refrigeration systems the following eight optimal cascaded vapor compression refrigeration systems have been considered for numerical computations.

System-1: Cascaded vapor compression refrigeration system using ecofriendly low GWP R450A refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{\text{Eva_LTC}}=35.167$ kW, $T_{\text{cond}}=50^{\circ}\text{C}$, $T_{\text{ambient}}=25^{\circ}\text{C}$, $T_{\text{Eva_HTC}}=-30^{\circ}\text{C}$, $T_{\text{Eva_LTC}}=-90^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

System- 2: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R513A refrigerants in higher temperature cycle using ecofriendly R452B low GWP refrigerant in low temperature cycle ($Q_{\text{Eva_LTC}}=35.167$ kW, $T_{\text{cond}}=50^{\circ}\text{C}$, $T_{\text{ambient}}=25^{\circ}\text{C}$, $T_{\text{Eva_HTC}}=-30^{\circ}\text{C}$, $T_{\text{Eva_LTC}}=-90^{\circ}\text{C}$, Temperature overlapping =10, Compressor efficiency_{HTC} =80%, Compressor efficiency_{LTC} =80%,}}

System-3: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R452B refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{\text{Eva_LTC}}=35.167$ kW, $T_{\text{cond}}=50^{\circ}\text{C}$, $T_{\text{ambient}}=25^{\circ}\text{C}$, $T_{\text{Eva_HTC}}=-30^{\circ}\text{C}$, $T_{\text{Eva_LTC}}=-90^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC} =80%, Compressor efficiency_{LTC}=80%,}}

System-4: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R452C refrigerants in higher temperature cycle using

ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-90^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

System-5: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R448A refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-90^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

System-6: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R449A refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-90^{\circ}C$, Temperature

overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

System-7: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R452A refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-90^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

System-8: Cascaded thermodynamic performances of vapor compression refrigeration system using ecofriendly low GWP R452B refrigerants in higher temperature cycle using ecofriendly R513A low GWP refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-90^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

Table-1(a) Thermodynamic performances of optimum combinations of cascaded VCERS using low GWP R454C refrigerants in higher temperature cycle using low GWP HFC+HFO blends in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=0^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| Cascaded VCERS | System 1 | System 2 | System 3 | System 4 | System 5 | System 6 | System 7 | System 8 |
|--|----------|----------|----------|----------|----------|----------|----------|----------|
| HFC +HFO Blends in HTC | R450A | R513A | R454B | R454C | R448A | R449A | R452A | R452B |
| HFC +HFO Blends in LTC | R513a | R452b | R513a | R513a | R513A | R513A | R513A | R513A |
| First Law Cascaded Efficiency COP _{Cascade} | 0.7711 | 0.7811 | 0.7544 | 0.7106 | 0.7394 | 0.7288 | 0.7606 | 0.7031 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.773 | 1.738 | 1.835 | 2.009 | 1.892 | 1.934 | 1.812 | 2.042 |
| Cascaded Exergetic Efficiency | 0.3606 | 0.3653 | 0.3528 | 0.3323 | 0.3458 | 0.3408 | 0.3557 | 0.3288 |
| Exergy of Fuel "kW" | 45.61 | 45.02 | 46.62 | 49.49 | 47.56 | 48.25 | 46.24 | 50.02 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5276 | 0.5761 | 0.3552 | 0.4979 | 0.4717 | 0.5007 | 0.3510 | 0.7087 |
| LTC Mass flow Rate (Kg/sec) | 0.2992 | 0.1672 | 0.2992 | 0.2992 | 0.2992 | 0.2992 | 0.2992 | 0.2992 |
| W _{comp_HTC} "kW" | 19.65 | 19.64 | 20.66 | 23.53 | 21.60 | 22.29 | 20.28 | 24.06 |
| W _{comp_LTC} "kW" | 25.96 | 25.39 | 25.96 | 25.96 | 25.96 | 25.96 | 25.96 | 25.96 |
| Q _{Cond_HTC} "kW" | 80.77 | 80.19 | 81.78 | 84.65 | 82.73 | 83.42 | 81.40 | 85.19 |
| Q _{Cond_LTC} "kW" | 61.12 | 60.55 | 61.12 | 61.12 | 61.12 | 61.12 | 61.12 | 61.12 |
| Q _{Eva_HTC} "kW" | 61.12 | 48.67 | 61.12 | 61.12 | 61.12 | 61.12 | 61.12 | 61.12 |
| Q _{Eva_LTC} "kW" | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 1.355 | 1.385 | 1.355 | 1.355 | 1.355 | 1.355 | 1.355 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 3.111 | 3.084 | 2.959 | 2.598 | 2.660 | 2.660 | 3.014 | 2.54 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.502 | 2.543 | 2.693 | 3.206 | 2.861 | 2.985 | 2.625 | 3.301 |
| HTC Exergetic Efficiency | 0.2847 | 0.2822 | 0.2708 | 0.2378 | 0.2590 | 0.2590 | 0.2759 | 0.2325 |
| HTC Exergy of Fuel "kW" | 19.65 | 19.64 | 20.66 | 23.63 | 21.60 | 22.29 | 20.28 | 24.06 |
| HTC Exergy of Product "kW" | 5.594 | 5.542 | 5.594 | 5.594 | 5.594 | 5.594 | 5.594 | 5.594 |

Table-1(a) shows the comparison of static thermodynamic performances of cascaded vapor compression refrigeration systems using eight different combinations of HFC +HFO Blends in high temperature cycle at -30°C in HTC evaporator and two different HFC +HFO Blends (R513a and R R452a) in low temperature cycle and it was found that optimal cascaded vapor compression refrigeration system-2 using R454B in high temperature cycle and R513A in low temperature cycle gives

highest first law efficiency and exergetic efficiency with lower power consumption in the both compressors along with lowest system exergy destruction ratio. Similar trends were observed in the thermodynamic system first law (energy) performance (COP_{Cascade}) and exergetic performance at evaporator temperature -5°C in table-1(b) and at HTC evaporator temperature of -30°C and LTC evaporator temperature of -70°C as shown in table-1(C) respectively.

Table-1(b) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R454C refrigerants in higher temperature cycle using low GWP HFC+HFO blends in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-5^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| Cascaded VCRS | System:1 | System 2 | System 3 | System: 4 | System 5 | System 6 | System 7 | System: 8 |
|--|----------|----------|----------|-----------|----------|----------|----------|-----------|
| HFC +HFO Blends in HTC | R450A | R513A | R454B | R454C | R448A | R449A | R452A | R452B |
| HFC +HFO Blends in LTC | R513a | R452b | R513a | R513a | R513A | R513A | R513A | R513A |
| First Law Cascaded Efficiency COP _{Cascade} | 0.7805 | 0.7827 | 0.76498 | 0.7143 | 0.7482 | 0.7358 | 0.7723 | 0.7637 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.740 | 1.732 | 1.796 | 1.985 | 1.858 | 1.906 | 1.762 | 2.039 |
| Cascaded Exergetic Efficiency | 0.3650 | 0.3660 | 0.3577 | 0.3350 | 0.3499 | 0.3441 | 0.3612 | 0.3291 |
| Exergy of Fuel “kW” | 45.06 | 44.93 | 45.97 | 49.10 | 47.0 | 47.0 | 45.54 | 49.97 |
| Exergy of Product “kW” | 16.46 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5201 | 0.5708 | 0.3436 | 0.5203 | 0.4609 | 0.4894 | 0.3395 | 0.6990 |
| LTC Mass flow Rate (Kg/sec) | 0.283 | 0.1608 | 0.2830 | 0.2830 | 0.2830 | 0.2830 | 0.2830 | 0.2830 |
| W _{comp_HTC} “kW” | 21.71 | 21.87 | 22.63 | 2575 | 23.66 | 24.45 | 22.19 | 26.63 |
| W _{comp_LTC} “kW” | 23.35 | 23.07 | 23.35 | 23.35 | 23.35 | 23.35 | 23.35 | 23.35 |
| Q _{Cond_HTC} “kW” | 80.23 | 80.10 | 81.14 | 84.26 | 82.17 | 82.96 | 80.7 | 85.14 |
| Q _{Cond_LTC} “kW” | 58.51 | 58.51 | 58.51 | 58.51 | 58.51 | 58.51 | 58.51 | 58.51 |
| Q _{Eva_HTC} “kW” | 48.39 | 58.51 | 58.51 | 58.51 | 48.39 | 48.39 | 58.51 | 58.51 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 1.506 | 1.506 | 1.506 | 1.506 | 1.506 | 1.506 | 1.506 | 1.506 |
| First Law HTC Efficiency COP _{HTC} | 2.695 | 2.663 | 2.586 | 2.272 | 2.272 | 2.473 | 2.637 | 2.197 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.317 | 2.356 | 2.457 | 2.934 | 2.934 | 2.614 | 2.390 | 3.068 |
| HTC Exergetic Efficiency | 0.3015 | 0.2980 | 0.2893 | 0.2542 | 0.2542 | 0.2767 | 0.2950 | 0.2458 |
| HTC Exergy of Fuel “kW” | 21.71 | 21.87 | 22.63 | 25.75 | 25.75 | 23.66 | 22.19 | 26.63 |
| HTC Exergy of Product “kW” | 6.546 | 6.546 | 6.546 | 6.546 | 6.546 | 6.546 | 6.546 | 6.546 |

Table-1(c) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R454C refrigerants in higher temperature cycle using low GWP HFC+HFO blends (refrigerants) in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| Cascaded VCRS | System:1 | System 2 | System 3 | System: 4 | System 5 | System 6 | System 7 | System: 8 |
|--|----------|----------|----------|-----------|----------|----------|----------|-----------|
| HFC +HFO Blends in HTC | R450A | R513A | R454B | R454C | R448A | R449A | R452A | R452B |
| HFC +HFO Blends in LTC | R513a | R452b | R513a | R513a | R513A | R513A | R513A | R513A |
| First Law Cascaded Efficiency COP _{Cascade} | 0.7425 | 0.7213 | 0.7487 | 0.6709 | 0.7153 | 0.6969 | 0.6293 | 0.7103 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.680 | 1.965 | 1.856 | 2.187 | 1.99 | 2.069 | 2.398 | 1.812 |
| Cascaded Exergetic Efficiency | 0.3472 | 0.3373 | 0.3501 | 0.3138 | 0.3345 | 0.3259 | 0.2936 | 0.3556 |
| Exergy of Fuel “kW” | 47.36 | 48.76 | 46.97 | 52.41 | 49.17 | 50.46 | 56.01 | 46.25 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5066 | 0.5653 | 0.3035 | 0.4979 | 0.4320 | 0.4575 | 0.6919 | 0.3010 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.1359 | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} “kW” | 34.12 | 35.25 | 33.75 | 39.19 | 35.94 | 37.24 | 42.79 | 33.03 |
| W _{comp_LTC} “kW” | 13.22 | 13.51 | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 82.53 | 83.92 | 82.14 | 87.58 | 84.33 | 85.63 | 91.18 | 81.42 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.67 | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.67 | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.660 | 2.604 | 2.66 | 2.660 | 2.660 | 2.660 | 2.660 | 2.660 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.381 | 1.434 | 1.235 | 1.346 | 1.299 | 1.131 | 1.465 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.199 | 2.202 | 2.083 | 2.581 | 2.284 | 2.402 | 2.909 | 2.017 |
| HTC Exergetic Efficiency | 0.3206 | 0.3123 | 0.3243 | 0.2793 | 0.3045 | 0.2939 | 0.2558 | 0.3314 |
| HTC Exergy of Fuel “kW” | 34.14 | 35.25 | 33.75 | 39.19 | 35.94 | 37.24 | 42.79 | 33.03 |
| HTC Exergy of Product “kW” | 10.95 | 11.01 | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

2.2 Dynamic thermodynamic(energy) and exergetic performances cascaded VCRS using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle (System-1)

It was found that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing. Similarly, by increasing LTC evaporator temperature from -50°C to -70°C, the first law (energy) performance (COP_{cascade}) is increasing and exergetic

performance is decreasing as shown in table-2(a) respectively. By increasing HTC condenser temperature from 40°C to 60°C, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-2(c) respectively.

Similarly by increasing temperature overlapping, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in table-2(d) to table-2(f) respectively

Table-2(a) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R450A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| HTC Evaporator temperature (°C) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
|--|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7425 | 0.7602 | 0.7733 | 0.7813 | 0.7838 | 0.7805 | 0.7711 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.880 | 1.813 | 1.765 | 1.737 | 1.728 | 1.740 | 1.773 |
| Cascaded Exergetic Efficiency | 0.3472 | 0.3555 | 0.3616 | 0.3653 | 0.3665 | 0.3650 | 0.3606 |
| Exergy of Fuel “kW” | 47.36 | 46.26 | 45.48 | 45.01 | 44.87 | 45.06 | 45.61 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.46 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5566 | 0.5068 | 0.5080 | 0.5106 | 0.5145 | 0.5201 | 0.5276 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.283 | 0.2992 |
| W _{comp_HTC} “kW” | 34.14 | 31.31 | 28.67 | 26.2 | 23.89 | 21.71 | 19.65 |
| W _{comp_LTC} “kW” | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q _{Cond_HTC} “kW” | 82.53 | 81.43 | 80.65 | 80.18 | 80.04 | 80.23 | 80.77 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 56.14 | 48.39 | 61.12 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.352 | 2.092 | 1.870 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.601 | 1.813 | 2.060 | 2.350 | 2.695 | 3.111 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.119 | 2.10 | 2.103 | 2.133 | 2.20 | 2.317 | 2.502 |
| HTC Exergetic Efficiency | 0.3206 | 0.3226 | 0.3223 | 0.3191 | 0.3125 | 0.3015 | 0.2847 |
| HTC Exergy of Fuel “kW” | 34.14 | 31.31 | 28.67 | 26.2 | 23.89 | 21.71 | 19.65 |
| HTC Exergy of Product “kW” | 10.95 | 10.10 | 9.329 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-2(b) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R450A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7425 | 0.7962 | 0.8526 | 0.9118 | 0.9739 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.880 | 1.905 | 1.941 | 1.991 | 2.055 |
| Cascaded Exergetic Efficiency | 0.3472 | 0.3443 | 0.340 | 0.3344 | 0.3273 |
| Exergy of Fuel “kW” | 47.36 | 44.17 | 41.25 | 38.57 | 36.11 |
| Exergy of Product “kW” | 16.45 | 15.21 | 14.02 | 12.9 | 11.82 |
| HTC Mass flow Rate (Kg/sec) | 0.5066 | 0.4870 | 0.4691 | 0.4526 | 0.4375 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.220 | 0.2556 | 0.2114 | 0.2074 |
| W _{comp_HTC} “kW” | 34.14 | 32.82 | 31.61 | 30.50 | 29.48 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 82.53 | 79.33 | 76.41 | 73.74 | 71.28 |
| Q _{Cond_LTC} “kW” | 48.38 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.38 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.417 | 1.417 | 1.417 | 1.417 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.119 | 2.119 | 2.119 | 2.119 | 2.119 |
| HTC Exergetic Efficiency | 0.3206 | 0.3206 | 0.3206 | 0.3206 | 0.3206 |
| HTC Exergy of Fuel “kW” | 34.14 | 32.82 | 31.61 | 30.50 | 29.48 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-2(c) Thermodynamic performances of optimum combinations of cascaded VCRES using low GWP R450A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | | |
|--|--------|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 60 | 55 | 50 | 45 | 40 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.6121 | 0.6768 | 0.7425 | 0.8019 | 0.8795 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.493 | 2.16 | 1.880 | 1.640 | 1.431 |
| Cascaded Exergetic Efficiency | 0.2863 | 0.3165 | 0.3472 | 0.3788 | 0.4113 |
| Exergy of Fuel “kW” | 57.45 | 51.96 | 47.36 | 43.42 | 39.98 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6035 | 0.5503 | 0.5066 | 0.470 | 0.4388 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} “kW” | 44.23 | 38.74 | 34.14 | 30.2 | 26.76 |
| W _{comp_LTC} “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 92.62 | 87.13 | 82.53 | 78.59 | 75.15 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.660 | 2.660 | 2.660 | 2.660 | 2.660 |
| First Law HTC Efficiency COP _{HTC} | 1.094 | 1.249 | 1.417 | 1.602 | 1.802 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 3.040 | 2.539 | 2.119 | 1.759 | 1.445 |
| HTC Exergetic Efficiency | 0.2475 | 0.2825 | 0.3206 | 0.3625 | 0.4090 |
| HTC Exergy of Fuel “kW” | 44.23 | 38.74 | 34.14 | 30.2 | 26.76 |
| HTC Exergy of Product “kW” | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

Table-2(d) Thermodynamic performances of optimum combinations of cascaded VCRES using low GWP R450A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | |
|--|--------|--------|--------|--------|
| Temperature overlapping (°C) | 0 | 5 | 10 | 15 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.8379 | 0.7887 | 0.7425 | 0.6989 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.552 | 1.711 | 1.880 | 2.06 |
| Cascaded Exergetic Efficiency | 0.3918 | 0.3688 | 0.3472 | 0.3268 |
| Exergy of Fuel “kW” | 41.97 | 44.59 | 47.36 | 50.31 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4735 | 0.4896 | 0.5066 | 0.5247 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} “kW” | 31.91 | 32.99 | 34.14 | 35.36 |
| W _{comp_LTC} “kW” | 10.06 | 11.60 | 13.22 | 14.95 |
| Q _{Cond_HTC} “kW” | 77.14 | 79.76 | 82.53 | 85.48 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.660 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.417 | 1.417 | 1.417 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.119 | 2.119 | 2.119 | 2.119 |
| HTC Exergetic Efficiency | 0.3206 | 0.3206 | 0.3206 | 0.3206 |
| HTC Exergy of Fuel “kW” | 31.91 | 32.99 | 34.14 | 35.36 |
| HTC Exergy of Product “kW” | 10.23 | 11.60 | 10.95 | 11.34 |

2.3 Dynamic thermodynamic(energy) and exergetic performances cascaded VCRES using ecofriendly low GWP R513a refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R450A refrigerant in low temperature cycle (system-2).

It was found that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing as shown in table-3(a) respectively. Similarly, by increasing LTC evaporator

temperature from -50°C to -70°C, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in table-3(b) respectively. By increasing HTC condenser temperature from 40oC to 60oC, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in table-3(c) respectively. Similarly, by increasing temperature overlapping, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in table-3(d) to table-3(e) respectively.

Table-2(e) Thermodynamic performances of optimum combinations of cascaded VCERS using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| Temperature overlapping ($^{\circ}C$) | 0 | 4 | 8 | 12 |
|--|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.8379 | 0.7903 | 0.7607 | 0.7248 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.552 | 1.679 | 1.811 | 1.95 |
| Cascaded Exergetic Efficiency | 0.3918 | 0.3733 | 0.3557 | 0.3389 |
| Exergy of Fuel “kW” | 41.97 | 44.05 | 46.23 | 0.4852 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4735 | 0.4863 | 0.4997 | 0.5137 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2142 | 0.2209 | 0.2281 |
| W _{comp_HTC} “kW” | 31.91 | 32.77 | 33.67 | 34.62 |
| W _{comp_LTC} “kW” | 10.06 | 11.28 | 12.56 | 13.90 |
| Q _{Cond_HTC} “kW” | 77.14 | 79.22 | 81.4 | 83.69 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.45 | 47.73 | 49.07 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.45 | 47.73 | 49.07 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.117 | 2.80 | 2.53 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.417 | 1.417 | 1.417 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.119 | 2.119 | 2.119 | 2.119 |
| HTC Exergetic Efficiency | 0.3206 | 0.3206 | 0.3206 | 0.3206 |
| HTC Exergy of Fuel “kW” | 31.91 | 32.77 | 33.67 | 34.62 |
| HTC Exergy of Product “kW” | 10.23 | 10.51 | 10.80 | 11.10 |

Table-2(f) Thermodynamic performances of optimum combinations of cascaded VCERS using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| Temperature overlapping ($^{\circ}C$) | 0.0 | 3 | 6 | 9 | 12 | 15 |
|--|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.8379 | 0.8080 | 0.7792 | 0.7515 | 0.7248 | 0.6989 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.552 | 1.647 | 1.744 | 1.845 | 1.95 | 2.06 |
| Cascaded Exergetic Efficiency | 0.3918 | 0.3778 | 0.3644 | 0.3514 | 0.3389 | 0.3268 |
| Exergy of Fuel “kW” | 41.97 | 43.52 | 45.13 | 46.79 | 0.4852 | 50.31 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4735 | 0.4831 | 0.4929 | 0.5031 | 0.5137 | 0.5247 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2126 | 0.2175 | 0.2227 | 0.2281 | 0.2339 |
| W _{comp_HTC} “kW” | 31.91 | 32.55 | 33.22 | 33.90 | 34.62 | 35.36 |
| W _{comp_LTC} “kW” | 10.06 | 10.97 | 11.91 | 12.89 | 13.90 | 14.95 |
| Q _{Cond_HTC} “kW” | 77.14 | 78.9 | 80.3 | 81.96 | 83.69 | 85.48 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.14 | 47.08 | 48.06 | 49.07 | 50.12 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.14 | 47.08 | 48.06 | 49.07 | 50.12 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.205 | 2.952 | 2.728 | 2.53 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.417 | 1.417 | 1.417 | 1.417 | 1.417 | 1.417 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.119 | 2.119 | 2.119 | 2.119 | 2.119 | 2.119 |
| HTC Exergetic Efficiency | 0.3206 | 0.3206 | 0.3206 | 0.3206 | 0.3206 | 0.3206 |
| HTC Exergy of Fuel “kW” | 31.91 | 32.55 | 33.22 | 33.90 | 34.62 | 35.36 |
| HTC Exergy of Product “kW” | 10.23 | 10.44 | 10.65 | 10.87 | 11.10 | 11.34 |

2.4 Dynamic thermodynamic (energy) and exergetic performances cascaded VCERS using ecofriendly low GWP R454B refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513A refrigerant in low temperature cycle(system-3)

It was found that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing as shown in Table-4(a) respectively. Similarly, by increasing LTC evaporator

temperature from $-50^{\circ}C$ to $-70^{\circ}C$, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in Table-4(b) respectively. By increasing HTC condenser temperature from $40^{\circ}C$ to $60^{\circ}C$, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-4(c) respectively. Similarly, by increasing temperature overlapping, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-4(d) respectively.

Table-3(a) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP GWP R513a refrigerant in HTC in higher temperature cycle using low GWP R452a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}\text{C}$, $T_{ambient}=25^{\circ}\text{C}$, $T_{Eva_LTC}=-70^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Evaporator Temperature ($^{\circ}\text{C}$) | -30 | -25 | -20 | -15 | -10 | -5 | -5 | 0 |
|--|--------|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7213 | 0.7419 | 0.7587 | 0.7713 | 0.7794 | 0.7827 | 0.7827 | 0.7811 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.965 | 1.882 | 1.818 | 1.772 | 1.744 | 1.732 | 1.732 | 1.738 |
| Cascaded Exergetic Efficiency | 0.3373 | 0.3470 | 0.3548 | 0.3607 | 0.3645 | 0.3660 | 0.3660 | 0.3653 |
| Exergy of Fuel "kW" | 48.76 | 47.40 | 46.35 | 45.59 | 45.12 | 44.93 | 44.93 | 45.02 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5653 | 0.5638 | 0.5636 | 0.5646 | 0.5670 | 0.5708 | 0.5708 | 0.5761 |
| LTC Mass flow Rate (Kg/sec) | 0.1359 | 0.1401 | 0.1447 | 0.1496 | 0.1550 | 0.1608 | 0.1608 | 0.1672 |
| W _{comp_HTC} "kW" | 35.25 | 32.2 | 29.36 | 26.71 | 24.22 | 21.87 | 21.87 | 19.64 |
| W _{comp_LTC} "kW" | 13.51 | 15.2 | 16.99 | 18.89 | 20.91 | 23.07 | 23.07 | 25.39 |
| Q _{Cond_HTC} "kW" | 83.92 | 82.57 | 81.52 | 80.76 | 80.29 | 80.10 | 80.10 | 80.19 |
| Q _{Cond_LTC} "kW" | 48.67 | 50.37 | 52.16 | 54.06 | 56.07 | 58.23 | 58.51 | 60.55 |
| Q _{Eva_HTC} "kW" | 48.67 | 50.37 | 52.16 | 54.06 | 56.07 | 58.23 | 58.51 | 48.67 |
| Q _{Eva_LTC} "kW" | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.604 | 2.313 | 2.070 | 1.862 | 1.682 | 1.525 | 1.506 | 1.385 |
| First Law HTC Efficiency COP _{HTC} | 1.381 | 1.564 | 1.777 | 2.024 | 2.317 | 2.663 | 2.663 | 3.084 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.202 | 2.173 | 2.167 | 2.189 | 2.247 | 2.356 | 2.356 | 2.543 |
| HTC Exergetic Efficiency | 0.2348 | 0.3153 | 0.3158 | 0.3136 | 0.3080 | 0.2980 | 0.2980 | 0.2822 |
| HTC Exergy of Fuel "kW" | 35.25 | 32.2 | 29.36 | 26.71 | 24.22 | 21.87 | 21.87 | 19.64 |
| HTC Exergy of Product "kW" | 11.01 | 10.15 | 9.272 | 8.376 | 7.458 | 6.515 | 6.546 | 5.542 |

Table-3(b) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R450A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}\text{C}$, $T_{ambient}=25^{\circ}\text{C}$, $T_{Eva_HTC}=-30^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| LTC Evaporator Temperature ($^{\circ}\text{C}$) | -70 | -65 | -60 | -55 | -50 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7213 | 0.7733 | 0.8277 | 8846 | 0.9441 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.965 | 1.991 | 2.03 | 2.083 | 2.151 |
| Cascaded Exergetic Efficiency | 0.3373 | 0.3343 | 0.3301 | 0.3244 | 0.3173 |
| Exergy of Fuel "kW" | 48.76 | 45.48 | 42.49 | 39.76 | 37.25 |
| Exergy of Product "kW" | 16.45 | 15.21 | 14.02 | 12.90 | 11.82 |
| HTC Mass flow Rate (Kg/sec) | 0.5653 | 0.5432 | 0.5231 | 0.5047 | 0.4878 |
| LTC Mass flow Rate (Kg/sec) | 0.1359 | 0.1341 | 0.1325 | 0.1309 | 0.1294 |
| W _{comp_HTC} "kW" | 35.25 | 33.87 | 32.62 | 31.47 | 30.42 |
| W _{comp_LTC} "kW" | 13.51 | 11.61 | 9.872 | 8.287 | 6.833 |
| Q _{Cond_HTC} "kW" | 83.92 | 80.65 | 77.66 | 74.92 | 72.42 |
| Q _{Cond_LTC} "kW" | 48.67 | 46.77 | 45.04 | 43.45 | 42.0 |
| Q _{Eva_HTC} "kW" | 48.67 | 46.77 | 45.04 | 43.45 | 42.0 |
| Q _{Eva_LTC} "kW" | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.604 | 3.03 | 3.562 | 4.244 | 5.147 |
| First Law HTC Efficiency COP _{HTC} | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 |
| HTC Exergetic Efficiency | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 |
| HTC Exergy of Fuel "kW" | 35.25 | 33.87 | 32.62 | 31.47 | 30.42 |
| HTC Exergy of Product "kW" | 11.01 | 10.58 | 10.19 | 9.829 | 9.50 |

Table-3(c) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP GWP R513a refrigerant in HTC in higher temperature cycle using low GWP R452b refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}\text{C}$, $T_{Eva_HTC}=-30^{\circ}\text{C}$, $T_{Eva_LTC}=-70^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature ($^{\circ}\text{C}$) | 60 | 55 | 50 | 45 | 40 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.5823 | 0.6515 | 0.7213 | 0.7921 | 0.8643 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.672 | 2.282 | 1.965 | 1.70 | 1.479 |
| Cascaded Exergetic Efficiency | 0.2723 | 0.3047 | 0.3379 | 0.3704 | 0.4040 |
| Exergy of Fuel "kW" | 60.39 | 57.97 | 48.76 | 44.39 | 40.67 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6918 | 0.6214 | 0.5653 | 0.5194 | 0.4811 |
| LTC Mass flow Rate (Kg/sec) | 0.1359 | 0.1359 | 0.1359 | 0.1359 | 0.1359 |
| W _{comp_HTC} "kW" | 46.89 | 40.47 | 35.25 | 30.89 | 27.16 |

| | | | | | |
|---|--------|--------|--------|--------|--------|
| W _{comp_LTC} “kW” | 13.51 | 13.51 | 13.51 | 13.51 | 13.51 |
| Q _{Cond_HTC} “kW” | 95.56 | 89.14 | 83.92 | 79.56 | 75.83 |
| Q _{Cond_LTC} “kW” | 48.67 | 48.67 | 48.67 | 48.67 | 48.67 |
| Q _{Eva_HTC} “kW” | 48.67 | 48.67 | 48.67 | 48.67 | 48.67 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.604 | 2.604 | 2.604 | 2.604 | 2.604 |
| First Law HTC Efficiency COP _{HTC} | 1.038 | 1.203 | 1.381 | 1.576 | 1.792 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 3.258 | 2.676 | 2.202 | 1.805 | 1.467 |
| HTC Exergetic Efficiency | 0.2348 | 0.2721 | 0.2348 | 0.3565 | 0.4054 |
| HTC Exergy of Fuel “kW” | 46.89 | 40.47 | 35.25 | 30.89 | 27.16 |
| HTC Exergy of Product “kW” | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 |

Table-3(d) Thermodynamic performances of optimum combinations of cascaded VCERS using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,}}

| Temperature overlapping (°C) | 0 | 4 | 5 | 8 | 10 | 12 | 15 |
|--|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.8115 | 0.7739 | 0.7648 | 0.7384 | 0.7213 | 0.7047 | 0.6805 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.635 | 1.763 | 1.796 | 1.896 | 1.965 | 2.035 | 2.142 |
| Cascaded Exergetic Efficiency | 0.3795 | 0.3619 | 0.3577 | 0.3453 | 0.3373 | 0.3295 | 0.3182 |
| Exergy of Fuel “kW” | 43.22 | 45.52 | 45.98 | 47.63 | 48.75 | 49.91 | 51.68 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5288 | 0.5429 | 0.5466 | 0.5577 | 0.5653 | 0.5730 | 0.5850 |
| LTC Mass flow Rate (Kg/sec) | 0.1282 | 0.1311 | 0.1319 | 0.1342 | 0.1359 | 0.1375 | 0.1401 |
| W _{comp_HTC} “kW” | 32.97 | 33.86 | 34.08 | 34.78 | 35.25 | 35.73 | 36.48 |
| W _{comp_LTC} “kW” | 10.36 | 11.58 | 10.90 | 12.85 | 13.51 | 14.17 | 15.20 |
| Q _{Cond_HTC} “kW” | 78.5 | 80.61 | 81.15 | 82.8 | 83.92 | 85.07 | 86.85 |
| Q _{Cond_LTC} “kW” | 45.53 | 46.75 | 47.06 | 48.02 | 48.67 | 49.34 | 50.37 |
| Q _{Eva_HTC} “kW” | 45.53 | 46.75 | 47.06 | 48.02 | 48.67 | 49.34 | 50.37 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.394 | 3.036 | 2.956 | 2.736 | 2.604 | 2.481 | 2.313 |
| First Law HTC Efficiency COP _{HTC} | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 |
| HTC Exergetic Efficiency | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 |
| HTC Exergy of Fuel “kW” | 32.97 | 33.86 | 34.08 | 34.78 | 35.25 | 35.73 | 36.48 |
| HTC Exergy of Product “kW” | 10.3 | 10.57 | 10.65 | 10.86 | 13.51 | 11.16 | 11.39 |

Table-3(e) Thermodynamic performances of optimum combinations of cascaded VCERS using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,}}

| Temperature overlapping (°C) | 0 | 3 | 6 | 9 | 12 | 15 |
|--|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.8115 | 0.7831 | 0.7559 | 0.7298 | 0.7047 | 0.6805 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.635 | 1.731 | 1.829 | 1.930 | 2.035 | 2.142 |
| Cascaded Exergetic Efficiency | 0.3795 | 0.3662 | 0.3535 | 0.3413 | 0.3295 | 0.3182 |
| Exergy of Fuel “kW” | 43.22 | 44.91 | 46.52 | 48.19 | 49.91 | 51.68 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5288 | 0.5393 | 0.5502 | 0.5615 | 0.5730 | 0.5850 |
| LTC Mass flow Rate (Kg/sec) | 0.1282 | 0.1304 | 0.1327 | 0.1350 | 0.1375 | 0.1401 |
| W _{comp_HTC} “kW” | 32.97 | 33.63 | 34.31 | 35.01 | 35.73 | 36.48 |
| W _{comp_LTC} “kW” | 10.36 | 11.27 | 12.21 | 13.18 | 14.17 | 15.20 |
| Q _{Cond_HTC} “kW” | 78.5 | 80.7 | 81.69 | 83.36 | 85.07 | 86.85 |
| Q _{Cond_LTC} “kW” | 45.53 | 46.44 | 47.38 | 48.35 | 49.34 | 50.37 |
| Q _{Eva_HTC} “kW” | 45.53 | 46.44 | 47.38 | 48.35 | 49.34 | 50.37 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.394 | 3.119 | 2.880 | 2.669 | 2.481 | 2.313 |
| First Law HTC Efficiency COP _{HTC} | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 | 1.381 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 | 2.202 |
| HTC Exergetic Efficiency | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 | 0.3123 |
| HTC Exergy of Fuel “kW” | 32.97 | 33.63 | 34.31 | 35.01 | 35.73 | 36.48 |
| HTC Exergy of Product “kW” | 10.3 | 10.50 | 10.72 | 10.94 | 11.16 | 11.39 |

Table-4(a) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R454B refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Evaporator Temperature ($^{\circ}C$) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
|--|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7487 | 0.7601 | 0.7677 | 0.7713 | 0.7705 | 0.7649 | 0.7544 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.856 | 1.810 | 1.785 | 1.792 | 1.775 | 1.796 | 1.835 |
| Cascaded Exergetic Efficiency | 0.3501 | 0.3554 | 0.3590 | 0.3607 | 0.3603 | 0.3577 | 0.3528 |
| Exergy of Fuel “kW” | 46.97 | 46.27 | 45.81 | 45.59 | 45.64 | 45.97 | 46.62 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3035 | 0.3097 | 0.3167 | 0.3246 | 0.3334 | 0.3436 | 0.3552 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.2830 | 0.2992 |
| W _{comp_HTC} “kW” | 33.75 | 31.31 | 29.0 | 26.79 | 24.67 | 22.63 | 20.66 |
| W _{comp_LTC} “kW” | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q _{Cond_HTC} “kW” | 82.14 | 81.44 | 80.97 | 80.76 | 80.81 | 81.14 | 81.78 |
| Q _{Cond_LTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.434 | 1.601 | 1.792 | 2.015 | 2.276 | 2.586 | 2.959 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.083 | 2.101 | 2.139 | 2.203 | 2.303 | 2.457 | 2.693 |
| HTC Exergetic Efficiency | 0.3243 | 0.3225 | 0.3186 | 0.3122 | 0.3027 | 0.2893 | 0.2708 |
| HTC Exergy of Fuel “kW” | 33.75 | 31.31 | 29.0 | 26.79 | 24.67 | 22.63 | 20.66 |
| HTC Exergy of Product “kW” | 10.95 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-4(b) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R454B refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| LTC Evaporator Temperature ($^{\circ}C$) | -70 | -65 | -60 | -55 | -50 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7487 | 0.8030 | 0.8601 | 0.9201 | 0.9831 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.856 | 1.88 | 1.916 | 1.964 | 2.027 |
| Cascaded Exergetic Efficiency | 0.3501 | 0.3472 | 0.3430 | 0.3374 | 33.04 |
| Exergy of Fuel “kW” | 46.97 | 43.79 | 40.89 | 40.49 | 35.77 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3035 | 0.2918 | 0.281 | 0.2712 | 0.2621 |
| LTC Mass flow Rate (Kg/sec) | 0.2345 | 0.220 | 0.2156 | 0.2114 | 0.2076 |
| W _{comp_HTC} “kW” | 33.75 | 32.44 | 31.25 | 30.15 | 29.15 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 82.14 | 78.96 | 76.05 | 73.39 | 70.94 |
| Q _{Cond_LTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 3.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.434 | 1.434 | 1.434 | 1.434 | 1.434 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.083 | 2.083 | 2.083 | 2.083 | 2.083 |
| HTC Exergetic Efficiency | 0.3243 | 0.3243 | 0.3243 | 0.3243 | 0.3243 |
| HTC Exergy of Fuel “kW” | 33.75 | 32.44 | 31.25 | 30.15 | 29.15 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-4(c) Thermodynamic performances of optimum combinations of cascaded VCRS (System-3) using low GWP R454B refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, , Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature ($^{\circ}C$) | 60 | 55 | 50 | 45 | 40 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.6185 | 0.6838 | 0.7487 | 0.8145 | 0.8817 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.457 | 2.127 | 1.856 | 1.626 | 1.425 |
| Cascaded Exergetic Efficiency | 0.2892 | 0.3198 | 0.3501 | 0.3808 | 0.4123 |
| Exergy of Fuel “kW” | 56.86 | 51.43 | 46.97 | 43.18 | 39.89 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3559 | 0.3267 | 0.3035 | 0.2845 | 0.2685 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |

| | | | | | |
|---|--------|--------|--------|--------|--------|
| W _{comp_HTC} “kW” | 43.63 | 38.21 | 33.75 | 29.96 | 26.66 |
| W _{comp_LTC} “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 92.02 | 86.60 | 82.14 | 78.39 | 75.05 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.16 | 35.16 | 35.16 | 35.16 | 35.16 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| First Law HTC Efficiency COP _{HTC} | 1.109 | 1.267 | 1.434 | 1.615 | 1.815 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.986 | 2.127 | 2.083 | 1.737 | 1.425 |
| HTC Exergetic Efficiency | 0.2509 | 0.2865 | 0.3243 | 0.3653 | 0.4123 |
| HTC Exergy of Fuel “kW” | 43.63 | 38.21 | 33.75 | 29.96 | 26.66 |
| HTC Exergy of Product “kW” | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

Table-4(d) Thermodynamic performances of optimum combinations of cascaded VCRCs using low GWP R454b refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | |
|--|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 0 | 5 | 10 | 15 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.8452 | 0.7954 | 0.7487 | 0.7046 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.53 | 1.688 | 1.856 | 2.035 |
| Cascaded Exergetic Efficiency | 0.3952 | 0.3720 | 0.3501 | 0.3295 |
| Exergy of Fuel “kW” | 41.61 | 44.21 | 46.97 | 49.91 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.2837 | 0.2933 | 0.3035 | 0.3144 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} “kW” | 31.55 | 32.62 | 33.75 | 34.96 |
| W _{comp_LTC} “kW” | 10.06 | 11.60 | 13.22 | 14.55 |
| Q _{Cond_HTC} “kW” | 76.27 | 79.38 | 82.14 | 85.08 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.434 | 1.434 | 1.434 | 1.434 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.083 | 2.083 | 2.083 | 2.083 |
| HTC Exergetic Efficiency | 0.3243 | 0.3243 | 0.3243 | 0.3243 |
| HTC Exergy of Fuel “kW” | 31.55 | 32.62 | 33.75 | 34.96 |
| HTC Exergy of Product “kW” | 10.23 | 10.58 | 10.95 | 11.34 |

2.5 Dynamic thermodynamic(energy) and exergetic performances cascaded VCRCs using ecofriendly low GWP R454C refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513A refrigerant in low temperature cycle(system-4)

It was observed that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing as shown in Table-5(a) respectively. Similarly, by increasing LTC evaporator

temperature from -50°C to -70°C, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in Table-5(b) respectively. By increasing HTC condenser temperature from 40°C to 60°C, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-5(c) respectively. Similarly by increasing temperature overlapping, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-5(d) respectively

Table-5(a) Thermodynamic performances of optimum combinations of cascaded VCRCs using low GWP R454C refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | | | | |
|--|--------|--------|--------|--------|--------|--------|--------|
| HTC Evaporator Temperature (°C) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.6709 | 0.6885 | 0.7023 | 0.7118 | 0.7166 | 0.7143 | 0.7106 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.187 | 2.106 | 2.045 | 2.004 | 1.984 | 1.985 | 2.009 |
| Cascaded Exergetic Efficiency | 0.3138 | 0.3220 | 0.3284 | 0.3329 | 0.3351 | 0.3350 | 0.3323 |
| Exergy of Fuel “kW” | 52.41 | 51.07 | 50.07 | 49.41 | 49.08 | 49.10 | 49.49 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 4979 | 4995 | 0.5023 | 0.5066 | 0.5125 | 0.5203 | 0.4979 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.2830 | 0.2992 |

| | | | | | | | |
|---|--------|--------|--------|--------|--------|--------|--------|
| W _{comp_HTC} “kW” | 39.19 | 36.12 | 33.26 | 30.60 | 28.10 | 2575 | 23.53 |
| W _{comp_LTC} “kW” | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q _{Cond_HTC} “kW” | 87.58 | 86.24 | 85.24 | 84.57 | 84.24 | 84.26 | 84.65 |
| Q _{Cond_LTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.660 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.235 | 1.388 | 1.563 | 1.764 | 1.998 | 2.272 | 2.598 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.581 | 2.577 | 2.60 | 2.659 | 2.763 | 2.934 | 3.206 |
| HTC Exergetic Efficiency | 0.2793 | 0.2796 | 0.2778 | 0.2733 | 0.2657 | 0.2542 | 0.2378 |
| HTC Exergy of Fuel “kW” | 39.19 | 36.12 | 33.26 | 30.60 | 28.10 | 25.75 | 23.63 |
| HTC Exergy of Product “kW” | 10.95 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-5(b) Thermodynamic performances of optimum combinations of cascaded VCRCs using low GWP R454C refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| | | | | | |
|--|--------|--------|--------|--------|--------|
| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
| First Law Cascaded Efficiency COP _{Cascade} | 6709 | 0.7173 | 0.7657 | 8162 | 0.8689 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.187 | 2.224 | 2.275 | 2.341 | 2.424 |
| Cascaded Exergetic Efficiency | 0.3136 | 0.3102 | 0.3054 | 0.2993 | 0.2920 |
| Exergy of Fuel “kW” | 52.41 | 49.03 | 45.93 | 43.09 | 40.47 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4979 | 0.4787 | 0.461 | 0.4448 | 0.430 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.220 | 0.2156 | 0.2114 | 0.2074 |
| W _{comp_HTC} “kW” | 39.19 | 37.68 | 36.29 | 35.02 | 33.85 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 87.58 | 84.19 | 81.09 | 78.25 | 75.64 |
| Q _{Cond_LTC} “kW” | 48.39 | 43.29 | 44.80 | 43.29 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.39 | 43.29 | 44.80 | 43.29 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.235 | 1.235 | 1.235 | 1.235 | 1.235 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.581 | 2.581 | 2.581 | 2.581 | 2.581 |
| HTC Exergetic Efficiency | 0.2793 | 0.2793 | 0.2793 | 0.2793 | 0.2793 |
| HTC Exergy of Fuel “kW” | 39.19 | 37.68 | 36.29 | 35.02 | 33.85 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-5(c) Thermodynamic performances of optimum combinations of cascaded VCRCs (System-4) using low GWP R454C refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| | | | | | |
|--|--------|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 60 | 55 | 50 | 45 | 40 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.5382 | 0.6050 | 0.6709 | 0.7370 | 0.8039 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.973 | 2.535 | 2.187 | 1.901 | 1.660 |
| Cascaded Exergetic Efficiency | 0.2517 | 0.2829 | 0.3138 | 0.3447 | 0.3759 |
| Exergy of Fuel “kW” | 65.34 | 58.13 | 52.41 | 47.72 | 43.74 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6136 | 0.5484 | 0.4979 | 0.4575 | 0.4242 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} “kW” | 52.12 | 44.91 | 39.19 | 34.49 | 30.52 |
| W _{comp_LTC} “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 100.5 | 93.30 | 87.58 | 82.88 | 79.91 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.660 | 2.660 | 2.660 | 2.660 | 2.660 |
| First Law HTC Efficiency COP _{HTC} | 0.9285 | 1.078 | 1.235 | 1.403 | 1.585 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 3.762 | 3.103 | 2.581 | 2.151 | 1.788 |
| HTC Exergetic Efficiency | 0.210 | 0.2437 | 0.2793 | 0.3173 | 0.3586 |
| HTC Exergy of Fuel “kW” | 52.12 | 44.91 | 39.19 | 34.49 | 30.52 |

Table-5(d) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R454C refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}\text{C}$, $T_{ambient}=25^{\circ}\text{C}$, $T_{Eva_HTC}=-30^{\circ}\text{C}$, $T_{Eva_LTC}=-70^{\circ}\text{C}$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| Temperature overlapping ($^{\circ}\text{C}$) | 0 | 5 | 10 | 15 |
|--|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7531 | 0.7108 | 0.6709 | 0.6335 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.839 | 2.008 | 2.187 | 2.378 |
| Cascaded Exergetic Efficiency | 0.3522 | 0.3324 | 0.3138 | 0.2961 |
| Exergy of Fuel "kW" | 46.69 | 49.47 | 52.41 | 55.55 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4654 | 0.4812 | 0.4979 | 0.5158 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} "kW" | 36.63 | 37.88 | 39.19 | 40.59 |
| W _{comp_LTC} "kW" | 10.06 | 11.60 | 13.22 | 14.55 |
| Q _{Cond_HTC} "kW" | 81.86 | 84.64 | 87.58 | 90.72 |
| Q _{Cond_LTC} "kW" | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} "kW" | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} "kW" | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.235 | 1.235 | 1.235 | 1.235 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.581 | 2.581 | 2.581 | 2.581 |
| HTC Exergetic Efficiency | 0.2793 | 0.2793 | 0.2793 | 0.2793 |
| HTC Exergy of Fuel "kW" | 36.63 | 37.88 | 39.19 | 40.59 |
| HTC Exergy of Product "kW" | 10.23 | 10.58 | 10.95 | 11.34 |

Table-6(a) Thermodynamic performances of optimum combinations of cascaded VCRS using low GWP R448A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}\text{C}$, $T_{ambient}=25^{\circ}\text{C}$, $T_{Eva_LTC}=-70^{\circ}\text{C}$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| HTC Evaporator Temperature ($^{\circ}\text{C}$) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
|--|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7153 | 0.7310 | 0.7426 | 0.7495 | 0.7515 | 0.7482 | 0.7394 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.99 | 1.925 | 1.880 | 1.853 | 1.846 | 1.858 | 1.892 |
| Cascaded Exergetic Efficiency | 0.3345 | 0.3418 | 0.3472 | 0.3505 | 0.3514 | 0.3499 | 0.3458 |
| Exergy of Fuel "kW" | 49.17 | 48.11 | 47.36 | 46.92 | 46.80 | 47.0 | 47.56 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4320 | 0.4351 | 0.4394 | 0.4450 | 0.4521 | 0.4609 | 0.4717 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.2830 | 0.2992 |
| W _{comp_HTC} "kW" | 35.94 | 33.15 | 30.55 | 28.11 | 25.82 | 23.66 | 21.60 |
| W _{comp_LTC} "kW" | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q _{Cond_HTC} "kW" | 84.33 | 83.27 | 82.53 | 82.09 | 81.96 | 82.17 | 82.73 |
| Q _{Cond_LTC} "kW" | 48.39 | 50.12 | 51.98 | 53.91 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} "kW" | 48.39 | 50.12 | 51.98 | 53.91 | 56.14 | 48.39 | 61.12 |
| Q _{Eva_LTC} "kW" | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.346 | 1.512 | 1.701 | 1.92 | 2.174 | 2.272 | 2.660 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.284 | 2.283 | 2.307 | 2.361 | 2.458 | 2.934 | 2.861 |
| HTC Exergetic Efficiency | 0.3045 | 0.3046 | 0.3024 | 0.2975 | 0.2892 | 0.2542 | 0.2590 |
| HTC Exergy of Fuel "kW" | 35.14 | 33.15 | 30.55 | 28.11 | 25.82 | 25.75 | 21.60 |
| HTC Exergy of Product "kW" | 10.95 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

2.6 Dynamic thermodynamic and exergetic performances cascaded VCRS using low GWP R448A refrigerant in HTC in higher temperature cycle using low GWP R513A refrigerant in low temperature cycle(system-5)

Thermodynamic performances of cascaded VCRS using ecofriendly low GWP R448A refrigerant in HTC in higher temperature cycle and ecofriendly low GWP R513A refrigerant in low temperature cycle for varying evaporator temperature from 0°C to -30°C and it was found that when evaporator temperature is increasing the system first law

(energy) performance (COP_{cascade}) and exergetic performance is increasing as shown in Table-6(a) respectively. Similarly, by increasing LTC evaporator temperature from -50°C to -70°C , the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in Table-6(b) respectively. By increasing HTC condenser temperature from 40°C to 60°C , the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-6(c) respectively. Similarly by increasing temperature overlapping, the first law (energy) performance

(COP_cascade) and exergetic performance is decreasing as shown in Table-6(d) respectively.

Table-6(b) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R448A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
|---|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP_Cascade | 0.7153 | 0.7661 | 0.8194 | 0.8752 | 0.9336 |
| Exergy Destruction Ratio(EDR_Cascade) | 1.99 | 2.019 | 2.060 | 2.116 | 2.187 |
| Cascaded Exergetic Efficiency | 0.3345 | 0.3313 | 0.3268 | 0.3210 | 0.3138 |
| Exergy of Fuel “kW” | 49.17 | 45.9 | 42.92 | 40.18 | 37.67 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.432 | 0.4153 | 0.40 | 0.3860 | 0.3731 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.22 | 0.2156 | 0.2114 | 0.2074 |
| W_comp_HTC “kW” | 35.94 | 34.55 | 33.28 | 32.11 | 31.04 |
| W_comp_LTC “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q_Cond_HTC “kW” | 84.33 | 81.07 | 78.09 | 75.35 | 72.83 |
| Q_Cond_LTC “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q_Eva_HTC “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q_Eva_LTC “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP_LTC | 2.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP_HTC | 1.346 | 1.346 | 1.346 | 1.346 | 1.346 |
| HTC Exergy Destruction Ratio(EDR_HTC) | 2.284 | 2.284 | 2.284 | 2.284 | 2.284 |
| HTC Exergetic Efficiency | 0.3045 | 0.3045 | 0.3045 | 0.3045 | 0.3045 |
| HTC Exergy of Fuel “kW” | 35.94 | 34.55 | 33.28 | 32.11 | 31.04 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-6(c) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system(System-5) using ecofriendly low GWP R448A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature (°C) | 60 | 55 | 50 | 45 | 40 |
|---|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP_Cascade | 0.5894 | 0.6524 | 0.7153 | 0.7784 | 0.8439 |
| Exergy Destruction Ratio(EDR_Cascade) | 2.628 | 2.278 | 1.99 | 1.745 | 1.534 |
| Cascaded Exergetic Efficiency | 0.2756 | 0.3050 | 0.3345 | 0.3642 | 0.3946 |
| Exergy of Fuel “kW” | 59.66 | 53.91 | 49.17 | 45.15 | 41.67 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5136 | 0.4684 | 0.4320 | 0.4019 | 0.3766 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W_comp_HTC “kW” | 46.44 | 40.69 | 35.94 | 31.93 | 28.45 |
| W_comp_LTC “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q_Cond_HTC “kW” | 94.83 | 89.07 | 84.33 | 80.32 | 76.84 |
| Q_Cond_LTC “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q_Eva_HTC “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q_Eva_LTC “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP_LTC | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| First Law HTC Efficiency COP_HTC | 1.042 | 1.189 | 1.346 | 1.516 | 1.701 |
| HTC Exergy Destruction Ratio(EDR_HTC) | 2.628 | 2.717 | 2.284 | 1.917 | 1.599 |
| HTC Exergetic Efficiency | 0.2357 | 0.2690 | 0.3045 | 0.3428 | 0.3847 |
| HTC Exergy of Fuel “kW” | 46.44 | 40.69 | 35.94 | 31.93 | 28.45 |
| HTC Exergy of Product “kW” | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

2.7 Dynamic thermodynamic and exergetic performances cascaded using low GWP R449A refrigerant in HTC in higher temperature cycle using low GWP R513A refrigerant in low temperature cycle(system-6)

Table-7(a) and Table-7(b) show the Optimum thermodynamic performances of cascaded vapor compression refrigeration

system using ecofriendly low GWP R449A refrigerant in HTC in higher temperature cycle and ecofriendly low GWP R513A refrigerant in low temperature cycle for varying evaporator temperature from 0°C to -30°C and it was found that when evaporator temperature is increasing the system first law (energy) performance (COP_cascade) and exergetic performance is increasing as shown in Table-7(a) respectively.

Similarly, by increasing LTC evaporator temperature from -50°C to -70°C, the first law (energy) performance (COP_cascade) is increasing and exergetic performance is decreasing as shown in Table-7(b) respectively. By increasing HTC condenser temperature from 40°C to 60°C, the first law (energy) performance (COP_cascade) and exergetic

performance is decreasing as shown in Table-7(c) respectively. Similarly, by increasing temperature overlapping, the first law (energy) performance (COP_cascade) and exergetic performance is decreasing as shown in Table-7(d) respectively.

Table-6(d) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R448A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| Temperature overlapping (°C) | 0 | 5 | 10 | 15 |
|---|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP_Cascade | 0.8055 | 0.759 | 0.7153 | 0.6739 |
| Exergy Destruction Ratio(EDR_Cascade) | 1.655 | 1.817 | 1.990 | 2.193 |
| Cascaded Exergetic Efficiency | 0.3767 | 0.3549 | 0.3345 | 0.3151 |
| Exergy of Fuel “kW” | 43.66 | 46.33 | 49.39 | 52.18 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4038 | 0.4175 | 0.4320 | 0.4475 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W_comp_HTC “kW” | 33.60 | 34.74 | 35.94 | 37.23 |
| W_comp_LTC “kW” | 10.06 | 11.60 | 13.22 | 14.55 |
| Q_Cond_HTC “kW” | 78.82 | 81.5 | 84.33 | 87.35 |
| Q_Cond_LTC “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q_Eva_HTC “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q_Eva_LTC “kW” | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP_LTC | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP_HTC | 1.346 | 1.346 | 1.346 | 1.346 |
| HTC Exergy Destruction Ratio(EDR_HTC) | 2.284 | 2.284 | 2.284 | 2.284 |
| HTC Exergetic Efficiency | 0.3045 | 0.3045 | 0.3045 | 0.3045 |
| HTC Exergy of Fuel “kW” | 33.60 | 34.74 | 35.94 | 37.23 |
| HTC Exergy of Product “kW” | 10.23 | 10.58 | 10.95 | 11.34 |

Table-7(a) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R449A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%.

| HTC Evaporator Temperature (°C) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
|---|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP_Cascade | 0.6969 | 0.7133 | 0.7259 | 0.734 | 0.7375 | 0.7358 | 0.7288 |
| Exergy Destruction Ratio(EDR_Cascade) | 2.069 | 1.998 | 1.946 | 1.913 | 1.90 | 1.906 | 1.934 |
| Cascaded Exergetic Efficiency | 0.3299 | 0.3336 | 0.3394 | 0.3433 | 0.3449 | 0.3441 | 0.3408 |
| Exergy of Fuel “kW” | 50.46 | 49.30 | 48.95 | 47.91 | 47.69 | 47.0 | 48.25 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4575 | 0.4612 | 0.4662 | 0.4724 | 0.480 | 0.4894 | 0.5007 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 2.686 | 0.2830 | 0.2992 |
| W_comp_HTC “kW” | 37.34 | 34.25 | 31.64 | 29.10 | 26.71 | 24.45 | 22.29 |
| W_comp_LTC “kW” | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q_Cond_HTC “kW” | 85.63 | 84.47 | 83.62 | 83.06 | 82.85 | 82.96 | 83.42 |
| Q_Cond_LTC “kW” | 58.91 | 50.12 | 51.98 | 53.93 | 56.14 | 58.51 | 61.12 |
| Q_Eva_HTC “kW” | 58.91 | 50.12 | 51.98 | 53.93 | 56.14 | 48.39 | 61.12 |
| Q_Eva_LTC “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP_LTC | 2.66 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP_HTC | 1.299 | 1.459 | 1.643 | 1.855 | 2.102 | 2.473 | 2.660 |
| HTC Exergy Destruction Ratio(EDR_HTC) | 2.402 | 2.401 | 2.425 | 2.48 | 2.577 | 2.614 | 2.985 |
| HTC Exergetic Efficiency | 0.2939 | 0.2940 | 0.2920 | 0.2874 | 0.2939 | 0.2767 | 0.2590 |
| HTC Exergy of Fuel “kW” | 37.34 | 34.35 | 31.64 | 29.10 | 26.71 | 23.66 | 22.29 |
| HTC Exergy of Product “kW” | 10.95 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-7(b) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R449A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.6969 | 0.7458 | 0.7971 | 0.8506 | 0.9066 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.069 | 2.101 | 2.146 | 2.206 | 2.282 |
| Cascaded Exergetic Efficiency | 0.3299 | 0.3225 | 0.3179 | 0.3119 | 0.3047 |
| Exergy of Fuel “kW” | 50.46 | 47.15 | 44.12 | 41.34 | 38.79 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4575 | 0.4398 | 0.4236 | 0.4087 | 0.3951 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.220 | 0.2156 | 0.2114 | 0.2074 |
| W _{comp_HTC} “kW” | 37.34 | 35.8 | 34.48 | 33.27 | 32.16 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 85.63 | 82.32 | 79.29 | 76.51 | 73.96 |
| Q _{Cond_LTC} “kW” | 48.9 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.9 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 3.098 | 3.649 | 4.369 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.299 | 1.299 | 1.299 | 1.299 | 1.299 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.402 | 2.402 | 2.402 | 2.402 | 2.402 |
| HTC Exergetic Efficiency | 0.2939 | 0.2939 | 0.2939 | 0.2939 | 0.2939 |
| HTC Exergy of Fuel “kW” | 37.34 | 35.8 | 34.48 | 33.27 | 32.16 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-7(c) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system(System-6) using ecofriendly low GWP R449A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature (°C) | 60 | 55 | 50 | 45 | 40 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.5635 | 0.6306 | 0.6969 | 0.7634 | 0.8309 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.795 | 2.391 | 2.069 | 1.801 | 1.573 |
| Cascaded Exergetic Efficiency | 0.2635 | 0.2949 | 0.3259 | 0.3570 | 0.3886 |
| Exergy of Fuel “kW” | 62.41 | 55.77 | 50.46 | 46.07 | 42.32 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.5566 | 0.5009 | 0.4575 | 0.4224 | 0.3933 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} “kW” | 49.19 | 42.55 | 37.24 | 32.84 | 29.10 |
| W _{comp_LTC} “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 97.58 | 90.94 | 85.63 | 81.23 | 77.49 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| First Law HTC Efficiency COP _{HTC} | 0.9838 | 1.137 | 1.299 | 1.437 | 1.663 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 3.494 | 2.887 | 2.402 | 2.001 | 1.658 |
| HTC Exergetic Efficiency | 0.2225 | 0.2573 | 0.2939 | 0.3333 | 0.3762 |
| HTC Exergy of Fuel “kW” | 49.19 | 42.55 | 37.24 | 32.84 | 29.10 |
| HTC Exergy of Product “kW” | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

2.8 Dynamic thermodynamic and exergetic performances cascaded VCRCs using low GWP R452A refrigerant in HTC in higher temperature cycle using low GWP R513A refrigerant in low temperature cycle(system-7)

It was observed that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing as shown in Table-8(a) respectively. Similarly, by increasing LTC evaporator

temperature from -50°C to -70°C, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in Table-8(b) respectively. By increasing HTC condenser temperature from 40°C to 60°C, the first law performance and exergetic performance is decreasing as shown in Table-8(c) respectively. Similarly, by increasing temperature overlapping, the first law (energy) performance and exergetic performance is decreasing as shown in Table-8(d) respectively.

Table-7(d) Thermodynamic performances of optimum combinations of cascaded VCRES using low GWP R449A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| | | | | |
|--|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 0 | 5 | 10 | 15 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.7837 | 0.7390 | 0.6969 | 0.6570 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.729 | 1.894 | 2.069 | 2.255 |
| Cascaded Exergetic Efficiency | 0.3665 | 0.3456 | 0.3259 | 0.3072 |
| Exergy of Fuel “kW” | 44.87 | 47.59 | 50.46 | 53.53 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.4276 | 0.4421 | 0.4575 | 0.4738 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} “kW” | 34.81 | 35.99 | 37.24 | 38.57 |
| W _{comp_LTC} “kW” | 10.06 | 11.60 | 13.22 | 14.55 |
| Q _{Cond_HTC} “kW” | 80.04 | 82.75 | 85.63 | 88.7 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.299 | 1.299 | 1.299 | 1.299 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.402 | 2.402 | 2.402 | 2.402 |
| HTC Exergetic Efficiency | 0.2939 | 0.2939 | 0.2939 | 0.2939 |
| HTC Exergy of Fuel “kW” | 34.81 | 35.99 | 37.24 | 38.57 |
| HTC Exergy of Product “kW” | 10.23 | 10.58 | 10.95 | 11.34 |

Table-8(a) Thermodynamic performances of optimum combinations of cascaded VCRES using low GWP R452A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| | | | | | | | |
|--|--------|--------|--------|--------|--------|--------|--------|
| HTC Evaporator Temperature (°C) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.6279 | 0.6519 | 0.6720 | 0.6878 | 0.6985 | 0.7723 | 0.7606 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.406 | 2.28 | 2.182 | 2.109 | 2.026 | 1.762 | 1.812 |
| Cascaded Exergetic Efficiency | 0.2936 | 0.3048 | 0.3143 | 0.3216 | 0.3266 | 0.3612 | 0.3557 |
| Exergy of Fuel “kW” | 56.10 | 53.95 | 52.33 | 51.13 | 50.35 | 45.54 | 46.24 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6919 | 0.6884 | 0.6873 | 0.6885 | 0.6924 | 0.3395 | 0.3510 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.2830 | 0.2992 |
| W _{comp_HTC} “kW” | 42.79 | 38.99 | 35.52 | 32.33 | 29.37 | 22.19 | 20.28 |
| W _{comp_LTC} “kW” | 13.22 | 14.95 | 16.81 | 18.81 | 20.98 | 23.35 | 25.96 |
| Q _{Cond_HTC} “kW” | 91.18 | 89.11 | 87.50 | 86.30 | 85.52 | 80.7 | 81.40 |
| Q _{Cond_LTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.131 | 1.285 | 1.463 | 1.67 | 1.911 | 2.637 | 3.014 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.909 | 2.28 | 2.844 | 2.865 | 2.933 | 2.390 | 2.625 |
| HTC Exergetic Efficiency | 0.2558 | 0.2590 | 0.2601 | 0.2587 | 0.2542 | 0.2950 | 0.2759 |
| HTC Exergy of Fuel “kW” | 42.79 | 38.99 | 35.52 | 32.33 | 29.37 | 22.19 | 20.28 |
| HTC Exergy of Product “kW” | 13.22 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-8(b) Thermodynamic performances of optimum combinations of cascaded VCRES system using low GWP R452A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| | | | | | |
|--|--------|--------|--------|--------|--------|
| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.6279 | 0.6701 | 0.7140 | 0.7596 | 0.8070 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.406 | 2.451 | 2.512 | 2.59 | 2.687 |
| Cascaded Exergetic Efficiency | 0.2936 | 0.2897 | 0.2840 | 0.2786 | 0.2712 |
| Exergy of Fuel “kW” | 56.01 | 52.48 | 49.24 | 46.30 | 43.58 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6919 | 0.6651 | 0.6406 | 0.6182 | 0.5976 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.220 | 0.2156 | 0.2114 | 0.2074 |

| | | | | | |
|---|--------|--------|--------|--------|--------|
| W _{comp_HTC} “kW” | 42.79 | 41.13 | 39.62 | 38.23 | 36.95 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 91.18 | 87.65 | 84.42 | 81.46 | 78.75 |
| Q _{Cond_LTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.131 | 1.131 | 1.131 | 1.131 | 1.131 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.909 | 2.909 | 2.909 | 2.909 | 2.909 |
| HTC Exergetic Efficiency | 0.2558 | 0.2558 | 0.2558 | 0.2558 | 0.2558 |
| HTC Exergy of Fuel “kW” | 42.79 | 41.13 | 39.62 | 38.23 | 42.79 |
| HTC Exergy of Product “kW” | 10.95 | 10.52 | 10.13 | 9.78 | 9.453 |

Table-8(c) Thermodynamic performances of optimum combinations of cascaded VCRS (System-7) using low GWP R452A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle (Q_{Eva_LTC}=35.167 kW, T_{ambient}=25°C, T_{Eva_HTC}=-30°C, T_{Eva_LTC}=-70°C, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | | |
|--|--------|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 60 | 55 | 50 | 45 | 40 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.4660 | 0.5487 | 0.6279 | 0.7055 | 0.7830 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 3.509 | 2.878 | 2.406 | 2.031 | 1.731 |
| Cascaded Exergetic Efficiency | 0.2179 | 0.2566 | 0.2936 | 0.3299 | 0.3662 |
| Exergy of Fuel “kW” | 75.47 | 64.10 | 56.01 | 49.84 | 44.91 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.9311 | 0.790 | 0.6919 | 0.6189 | 0.5620 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} “kW” | 62.25 | 50.87 | 42.79 | 36.62 | 31.69 |
| W _{comp_LTC} “kW” | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} “kW” | 110.6 | 99.26 | 91.18 | 85.01 | 80.08 |
| Q _{Cond_LTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} “kW” | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| First Law HTC Efficiency COP _{HTC} | 0.7774 | 0.9512 | 1.131 | 1.321 | 1.527 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 4.687 | 3.648 | 2.909 | 2.346 | 1.895 |
| HTC Exergetic Efficiency | 0.1758 | 0.2152 | 0.2558 | 0.2989 | 0.3454 |
| HTC Exergy of Fuel “kW” | 62.25 | 50.87 | 42.79 | 36.62 | 31.69 |
| HTC Exergy of Product “kW” | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

Table-8(d) Thermodynamic performances of optimum combinations of cascaded VCRS system using low GWP R452A refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle (Q_{Eva_LTC}=35.167 kW, T_{cond}=50°C, T_{ambient}=25°C, T_{Eva_HTC}=-30°C, T_{Eva_LTC}=-70°C, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| | | | | |
|--|--------|--------|--------|--------|
| HTC Condenser Temperature (°C) | 0 | 5 | 10 | 15 |
| First Law Cascaded Efficiency COP _{Cascade} | 0.7026 | 0.6642 | 0.6279 | 0.5933 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.044 | 2.220 | 2.406 | 2.604 |
| Cascaded Exergetic Efficiency | 0.3285 | 0.3106 | 0.2936 | 0.2775 |
| Exergy of Fuel “kW” | 50.05 | 52.95 | 56.01 | 0.5927 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.6467 | 0.6687 | 0.6919 | 0.7167 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} “kW” | 39.99 | 41.35 | 42.79 | 44.32 |
| W _{comp_LTC} “kW” | 10.06 | 11.60 | 13.22 | 14.55 |
| Q _{Cond_HTC} “kW” | 85.22 | 88.11 | 91.98 | 94.44 |
| Q _{Cond_LTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} “kW” | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.131 | 1.131 | 1.131 | 1.131 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.909 | 2.909 | 2.909 | 2.909 |
| HTC Exergetic Efficiency | 0.2558 | 0.2558 | 0.2558 | 0.2558 |
| HTC Exergy of Fuel “kW” | 39.99 | 41.35 | 42.79 | 44.32 |

2.9 Dynamic thermodynamic and exergetic performances cascaded VCERS using low GWP R452B refrigerant in HTC in higher temperature cycle using low GWP R513A refrigerant in low temperature cycle(system-7)

Thermodynamic performances of cascaded vapor compression refrigeration system using ecofriendly low GWP R452B refrigerant in HTC in higher temperature cycle and ecofriendly low GWP R513A refrigerant in low temperature cycle for varying evaporator temperature from 0°C to -30°C and it was found that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and

exergetic performance is increasing as shown in Table-9(a) respectively. Similarly, by increasing LTC evaporator temperature from -50°C to -70°C, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing as shown in Table-9(b) respectively. By increasing HTC condenser temperature from 40°C to 60°C, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-9(c) respectively. Similarly by increasing temperature overlapping, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing as shown in Table-9(d) respectively

Table-9(a) Thermodynamic performances of optimum combinations of cascaded VCERS using low GWP R452BA refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| HTC Evaporator Temperature (°C) | -30 | -25 | -20 | -15 | -10 | -5 | 0 |
|--|--------|--------|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.7603 | 0.7712 | 0.7782 | 0.7809 | 0.7790 | 0.7037 | 0.7031 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.812 | 1.773 | 1.748 | 1.739 | 2.237 | 2.039 | 2.042 |
| Cascaded Exergetic Efficiency | 0.3596 | 0.3607 | 0.3639 | 0.3652 | 0.3643 | 0.3291 | 0.3288 |
| Exergy of Fuel “kW” | 46.25 | 45.60 | 45.19 | 45.04 | 45.14 | 49.97 | 50.02 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3010 | 0.3068 | 0.3133 | 0.3209 | 0.3295 | 0.6990 | 0.7087 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2339 | 0.2443 | 0.2558 | 0.2686 | 0.2830 | 0.2992 |
| W _{comp_HTC} “kW” | 33.03 | 30.64 | 28.38 | 26.23 | 24.17 | 26.63 | 24.06 |
| W _{comp_LTC} “kW” | 20.98 | 18.81 | 16.81 | 14.95 | 13.22 | 23.35 | 25.96 |
| Q _{Cond_HTC} “kW” | 81.42 | 80.77 | 80.36 | 80.20 | 80.13 | 85.14 | 85.19 |
| Q _{Cond_LTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_HTC} “kW” | 48.39 | 50.12 | 51.98 | 53.97 | 56.14 | 58.51 | 61.12 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.352 | 2.092 | 1.87 | 1.677 | 1.506 | 1.355 |
| First Law HTC Efficiency COP _{HTC} | 1.465 | 1.636 | 1.831 | 2.058 | 2.323 | 2.197 | 2.54 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.017 | 2.034 | 2.072 | 2.136 | 2.237 | 3.068 | 3.301 |
| HTC Exergetic Efficiency | 0.3314 | 0.3296 | 0.3255 | 0.3652 | 0.3090 | 0.2458 | 0.2325 |
| HTC Exergy of Fuel “kW” | 33.03 | 30.64 | 28.38 | 26.23 | 24.17 | 26.63 | 24.06 |
| HTC Exergy of Product “kW” | 13.22 | 10.10 | 9.239 | 8.363 | 7.467 | 6.546 | 5.594 |

Table-9(b) Thermodynamic performances of optimum combinations of cascaded VCERS using low GWP R452B refrigerant in HTC in higher temperature cycle using low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%,

| LTC Evaporator Temperature (°C) | -70 | -65 | -60 | -55 | -50 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 1.0 | 0.9358 | 0.8744 | 0.8159 | 0.7603 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.812 | 1.835 | 1.868 | 1.914 | 1.914 |
| Cascaded Exergetic Efficiency | 0.3556 | 0.3528 | 0.3487 | 0.3432 | 0.3363 |
| Exergy of Fuel “kW” | 46.25 | 43.10 | 40.22 | 37.58 | 35.15 |
| Exergy of Product “kW” | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3010 | 0.2894 | 0.2787 | 0.2689 | 0.260 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.220 | 0.2156 | 0.2114 | 0.2074 |
| W _{comp_HTC} “kW” | 33.03 | 31.75 | 30.58 | 29.51 | 28.53 |
| W _{comp_LTC} “kW” | 13.22 | 11.35 | 9.638 | 8.068 | 6.625 |
| Q _{Cond_HTC} “kW” | 81.42 | 78.27 | 75.39 | 78.27 | 81.42 |
| Q _{Cond_LTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_HTC} “kW” | 48.39 | 46.52 | 44.80 | 43.23 | 41.79 |
| Q _{Eva_LTC} “kW” | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 3.098 | 3.649 | 4.359 | 5.308 |
| First Law HTC Efficiency COP _{HTC} | 1.465 | 1.465 | 1.465 | 1.465 | 1.465 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.017 | 2.017 | 2.017 | 2.017 | 2.017 |
| HTC Exergetic Efficiency | 0.3314 | 0.3314 | 0.3314 | 0.3314 | 0.3314 |
| HTC Exergy of Fuel “kW” | 33.03 | 31.75 | 30.58 | 29.51 | 28.53 |

Table-9(c) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R452B refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a(System-8) refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Temperature overlapping=10, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature ($^{\circ}C$) | 60 | 55 | 50 | 45 | 40 |
|--|--------|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.6307 | 0.6956 | 0.7603 | 0.8262 | 0.8939 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 2.39 | 2.074 | 1.812 | 1.588 | 1.392 |
| Cascaded Exergetic Efficiency | 0.2950 | 0.3253 | 0.3556 | 0.3863 | 0.4180 |
| Exergy of Fuel "kW" | 55.75 | 50.56 | 46.25 | 42.57 | 39.34 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.3502 | 0.3229 | 0.3010 | 0.2828 | 0.2673 |
| LTC Mass flow Rate (Kg/sec) | 0.2245 | 0.2245 | 0.2245 | 0.2245 | 0.2245 |
| W _{comp_HTC} "kW" | 42.53 | 37.34 | 33.03 | 29.34 | 26.12 |
| W _{comp_LTC} "kW" | 13.22 | 13.22 | 13.22 | 13.22 | 13.22 |
| Q _{Cond_HTC} "kW" | 90.92 | 85.73 | 81.42 | 77.73 | 74.51 |
| Q _{Cond_LTC} "kW" | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_HTC} "kW" | 48.39 | 48.39 | 48.39 | 48.39 | 48.39 |
| Q _{Eva_LTC} "kW" | 35.167 | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| First Law HTC Efficiency COP _{HTC} | 1.138 | 1.296 | 1.465 | 1.649 | 1.853 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.886 | 2.411 | 2.017 | 1.681 | 1.386 |
| HTC Exergetic Efficiency | 0.2574 | 0.2932 | 0.3314 | 0.3730 | 0.4191 |
| HTC Exergy of Fuel "kW" | 42.53 | 37.34 | 33.03 | 29.34 | 26.12 |
| HTC Exergy of Product "kW" | 10.95 | 10.95 | 10.95 | 10.95 | 10.95 |

Table-9(d) Thermodynamic performances of optimum combinations of cascaded vapor compression refrigeration system using ecofriendly low GWP R452b refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle ($Q_{Eva_LTC}=35.167$ kW, $T_{cond}=50^{\circ}C$, $T_{ambient}=25^{\circ}C$, $T_{Eva_HTC}=-30^{\circ}C$, $T_{Eva_LTC}=-70^{\circ}C$, Compressor efficiency_{HTC}=80%, Compressor efficiency_{LTC}=80%

| HTC Condenser Temperature ($^{\circ}C$) | 0 | 5 | 10 | 15 |
|--|--------|--------|--------|--------|
| First Law Cascaded Efficiency COP _{Cascade} | 0.8591 | 0.8080 | 0.7603 | 0.7153 |
| Exergy Destruction Ratio(EDR _{Cascade}) | 1.489 | 1.646 | 1.812 | 1.99 |
| Cascaded Exergetic Efficiency | 0.4018 | 0.3779 | 0.3556 | 0.3345 |
| Exergy of Fuel "kW" | 40.93 | 43.52 | 46.25 | 49.16 |
| Exergy of Product "kW" | 16.45 | 16.45 | 16.45 | 16.45 |
| HTC Mass flow Rate (Kg/sec) | 0.2813 | 0.2909 | 0.3010 | 0.3118 |
| LTC Mass flow Rate (Kg/sec) | 0.2079 | 0.2158 | 0.2245 | 0.2339 |
| W _{comp_HTC} "kW" | 30.87 | 31.922 | 33.03 | 34.21 |
| W _{comp_LTC} "kW" | 10.06 | 11.60 | 13.22 | 14.55 |
| Q _{Cond_HTC} "kW" | 76.10 | 78.68 | 81.42 | 84.33 |
| Q _{Cond_LTC} "kW" | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_HTC} "kW" | 45.23 | 46.76 | 48.39 | 50.12 |
| Q _{Eva_LTC} "kW" | 35.167 | 35.167 | 35.167 | 35.167 |
| First Law LTC Efficiency COP _{LTC} | 3.495 | 3.032 | 2.66 | 2.352 |
| First Law HTC Efficiency COP _{HTC} | 1.465 | 1.465 | 1.465 | 1.465 |
| HTC Exergy Destruction Ratio(EDR _{HTC}) | 2.017 | 2.017 | 2.017 | 2.017 |
| HTC Exergetic Efficiency | 0.3314 | 0.3314 | 0.3314 | 0.3314 |
| HTC Exergy of Fuel "kW" | 30.87 | 31.922 | 33.03 | 34.21 |

3. Conclusions

Following conclusions were made using HFC+HFO blends for Replacing R404a, R410a and R12, R22, R502, R507a

- Static thermodynamic performances of cascaded vapor compression refrigeration systems using eight different combinations of HFC +HFO Blends in high temperature cycle at $-30^{\circ}C$ in HTC evaporator and two different HFC +HFO Blends (R513a and R452a) in low temperature cycle and it was found that optimal cascaded vapor

compression refrigeration system-2 using R454B in high temperature cycle and R513A in low temperature cycle gives highest first law efficiency and exergetic efficiency with lower power consumption in the both compressors along with lowest system exergy destruction ratio. The lowest thermodynamic performances was observed by using ecofriendly low GWP R452A refrigerants in higher temperature cycle using ecofriendly R454B low GWP refrigerant in low temperature cycle in the Cascaded thermodynamic performances of vapor compression

refrigeration

- Cascaded vapor compression refrigeration system using R454B in high temperature cycle and R513A in low temperature cycle at -90°C gives higher first law efficiency and exergetic efficiency and lower exergy destruction ratio
- Dynamic Thermodynamic performances of cascaded vapor compression refrigeration system using ecofriendly low GWP R450A refrigerant in HTC in higher temperature cycle using ecofriendly low GWP R513a refrigerant in low temperature cycle and R513a refrigerant in low temperature cycle for varying evaporator temperature from 0°C to -30°C and it was found that when evaporator temperature is increasing the system first law (energy) performance (COP_{cascade}) and exergetic performance is increasing.
- By increasing LTC evaporator temperature from -50°C to -70°C in the all eight cascaded optimal vapor compression refrigeration systems, the first law (energy) performance (COP_{cascade}) is increasing and exergetic performance is decreasing
- By increasing HTC condenser temperature from 40°C to 60°C, in the all eight cascaded optimal vapor compression refrigeration systems, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing.
- By increasing temperature overlapping, in the all eight cascaded optimal vapor compression refrigeration

systems, the first law (energy) performance (COP_{cascade}) and exergetic performance is decreasing respectively

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